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City of Oxnard
Public Works Integrated Master Plan
RECYCLED WATER
PROJECT MEMORANDUM 4.4 ARC FLASH ASSESSMENT

FINAL DRAFT
December 2015


Engineers...Working Wonders With Water ${ }^{\text {™ }}$

City of Oxnard
Public Works Integrated Master Plan
RECYCLED WATER
PROJECT MEMORANDUM 4.4
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Project Memorandum 4.4

## ARC FLASH ASSESSMENT

### 1.0 INTRODUCTION

As part of the Public Works Integrated Master Plan (PWIMP), Power Studies.com was contracted to conduct assessments for short circuiting, protective device coordination, and arc flash potential for the Advanced Water Purification Facility (AWPF) and recycled water distribution system within the City of Oxnard (City). The summary report for all three of these studies is included in Appendix A.

### 1.1 PMs Used for Reference

The findings outlined in the Arc Flash Assessment were made in concert with recommendations and analyses from other related PMs:

- PM 4.1 - Recycled Water System - Background Summary.


### 2.0 FINDINGS

Below is a summary of the findings and recommendations for the City's recycled water infrastructure as it relates to the study noted above.

### 2.1 AWPF

- Arc Flash warning labels were provided for various locations to aid technicians in determining what PPE clothing should be worn.


### 2.2 Recycled Water Distribution System

- Revise, update and redraw the Distribution System One-Line Drawings for the facility when new equipment is added. This will decrease trouble-shooting time, reduce errors in decision-making, and decrease engineering costs for future projects.
- $\quad$ Verify that the device setting are set to the values shown in Appendix A, Tab 9.
- Test and inspect all electrical equipment periodically as outlined in applicable standards (as noted in report in Appendix A).

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## APPENDIX A - SHORT CIRCUIT, PROTECTION DEVICE COORDINATION AND ARC FLASH STUDIES

## SHORT CIRCUIT, PROTECTIVE DEVICE COORDINATION \& ARC FLASH STUDIES

## Oxnard Advanced Water Purification Oxnard, CA

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Customer P.O. \# 6200-10100-1093
Job \# 1104042-1


Date: 4/28/11
Revision 0

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TAB 1

## INTRODUCTION

In 2011, Doty Bros. Equipment Company was awarded a contract to provide the electrical distribution equipment for the Oxnard Advanced Water Purification. The facility is located in Oxnard, CA. The specifications for this project required a short circuit, protective device coordination, and arc flash studies.

A short circuit study was performed to determine the short circuit current values at various points throughout the distribution system. The short circuit data was collected from the existing equipment nameplates, drawings and submittals for the new equipment. These values were then compared to the equipment short circuit rating.

The study contains a reduced copy of the one-line drawing, and computer printouts of the fault values. A list of the equipment short circuit ratings is also included.

PowerStudies.com, P.S. also performed a protective device coordination study. This study determined circuit breaker settings and verified the fuse sizes. The coordination study can be found in Tab 7. The time current curves are located under Tab 8. The circuit breaker and relay setting sheets are located under Tab 9. Copies of the manufacturer's time current curves are found under Tab 10.

The protection engineer from PowerStudies.com also performed an Arc Flash Study for the distribution system shown on the one line drawing. The study calculated the Arc Flash Boundary, Incident Energy Level, and the required Personnel Protection Equipment (PPE). The study includes a spreadsheet-type listing of each piece of electrical equipment that would require servicing while energized, upstream protective devices, arc flash boundaries, incident energy, and required PPE; these are the Arc Flash Evaluation Bus and Protective device line side Reports. They are located in Tab 12. Paper copies of the Arc Flash labels located in Tab 13. (Note: Only 1 set of adhesive labels is included for this project.) These labels should be attached to each piece of equipment.

TAB 2

## EXECUTIVE SUMMARY AND RECOMMENDATIONS

The purpose of the short circuit study was to determine the available fault current at the switchgear, switchboards, panelboards, and other equipment throughout the facility. The engineer performed the short circuit study on the existing and new equipment being supplied. The engineer compared the fault values to the equipment short circuit rating.

The engineer calculated the fault current using the SKM computer program. This program ignores the current limiting effect of the fuses. If the equipment is underrated on a fully rated basis, then the engineer applies a series rating method. If a series rating method can not be applied and the equipment is pre-1982 design, then the Bussmann Up-and-Over and Up-Over-and Down Method is used. Flow chart \#2 shows this procedure and is included at the end of Tab 3.

The summary sheet in Tab 6 lists all equipment and short circuit ratings on a fully rated or series rated basis. Southern California Edison supplied the available fault current and transformer information. (3) 2500 kVA transformer with $5.75 \%$ impedance was supplied by Southern California Edison. The available fault current used in the study is listed below.

|  |  | Available Fault Current |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Node ID\# | Node Name | Volts | 3-Phase | Line to Grd |
| 05XFMR9001S | 05XFMR9001 SEC | 480 | $37,655 \mathrm{~A}$ | $41,533 \mathrm{~A}$ |
| 05XFMR9002S | 05XFMR9002 SEC | 480 | $37,655 \mathrm{~A}$ | $41,533 \mathrm{~A}$ |
| 05XFMR9004S | 05XFMR9004 SEC | 480 | $37,647 \mathrm{~A}$ | $41,526 \mathrm{~A}$ |

The study was performed on the existing and new equipment being installed. The calculations show that all the new equipment is properly rated for the available fault current.

PowerStudies.com, P.S. performed the coordination study to determine proper settings for the protective devices. PowerStudies.com, P.S. also provided recommendations for obtaining better equipment protection.

Selecting a proper setting is part art and part science. The engineer determined settings to increase protection and reduce the number of circuits that will de-energize due to a fault. The settings of these devices depend not only on engineering judgment, but also on personal experience and local operating conditions. Any appreciable change in system capacity, load, operating procedure, or short circuit characteristics requires a reexamination of breaker settings.

Due to the inherent nature of molded case circuit breakers and fuses, there was some inevitable overlapping between fuse and breaker instantaneous operation regions. These devices are sometimes impossible to coordinate, unless there is a large amount of impedance between upstream and downstream devices (i.e. transformers or long feeder

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lengths). This problem does not require any action. The industry considers this to be a tolerable situation except for elevator circuits and controllers.

The following recommendations will correct code violations and equipment problems.

1. The engineer was informed the breaker currently feeding the 15 kVA transformer on panel 40DP9202 is a 60A FD. This is a code violation as this is too high for a 15 kVA transformer. Consider replacing this with a 30A FD breaker.
2. The engineer was informed the breaker currently feeding the 15 kVA transformer on panel 30DP9201 is a 50A FD. This is a code violation as this is too high for a 15 kVA transformer. Consider replacing this with a 30A FD breaker.

PowerStudies.com performed arc flash calculations for the distribution system shown on the one line drawing. The arc flash calculations show that PPE clothing can be worn to increase personnel protection for the majority of the locations. The study was performed using the NFPA-70E (2004), IEEE - 1584 (2002), and NEC standards and codes. Using these standards along with the Power*Tools for Windows - Arc Flash Module, the engineer determined the incident energy level at various points throughout the distribution system.

The engineer performed the arc flash calculations for the equipment shown on the electrical one line drawing contained in the report. The engineer started at the utility main service and continued downstream but stopping at the secondary side of any 208 Volt transformers rated less than 125 kVA. This is based upon IEEE 1584 (2002) Standard page 15 that states, "Equipment below 240 V need not be considered unless it involves at least one 125 kVA or larger low impedance transformer in its immediate power supply". Page 34 of the Standard also states, "The arc-flash hazard need only be considered for large 208 V systems: systems fed by transformers smaller than 125 kVA should not be a concern." For these downstream areas, generic labels were created for these locations.

To aid the technicians in determining what PPE must be worn, Arc flash warning labels are provided for these various locations. The examples of these warning labels are shown below.


Figure 1 - Example Arc Flash Label

The PPE clothing class is determined based upon the incident energy and voltage class. The PPE matrix table (130.7(C)(10)) from NFPA 70E (2009) can be found in Tab 11.

The engineer assumed the maximum arcing time current would be two seconds as referenced in IEEE-1584-2002. This is a reasonable assumption because after this period, the individual would either move voluntarily or be blown clear of the arcing fault.

The arc flash calculations show that PPE clothing can be worn to increase personnel protection for most of the locations. Arc flash warning labels provided for these locations indicate the PPE required to be worn. The engineer recommends that the arc flash warning labels be installed on the electrical equipment to warn personnel of the potential hazard.

The following is a list of locations where the available incident energy exceeds 40 $\mathrm{Cal} / \mathrm{cm}^{\wedge} 2$. At these locations, the Required Protective FR Clothing Class is displayed as: "**** Dangerous!!! No FR Class Found. Before working on this equipment, the protection engineer strongly recommends that this equipment be de-energized.

## Maximum Arc Flash Energy (US) - Danger Only

## Scenario Descriptions <br> Scenario 1: Utility Power

## Calculation Details

IEEE 1584-2002/2004a Edition Bus + Line Side Report (Include Line Side + Load Side
Contributions), 80\% Cleared Fault Threshold, include Ind. Motors for 5.0 Cycles), mis-coordination checked

## Hazard Categories

Category 0: Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)
Category 1: FR Clothing Minimum Arc Rating of 4 (See NFPA 70E 130.7(C)(10) for additional PPE) Category 2: FR Clothing Minimum Arc Rating of 8 (See NFPA 70E 130.7(C)(10) for additional PPE)
Category 3: FR Clothing Minimum Arc Rating of 25 (See NFPA 70E 130.7(C)(10) for additional
PPE)
Category 4: FR Clothing Minimum Arc Rating of 40 (See NFPA 70E 130.7(C)(10) for additional
PPE)
DANGEROUS!: No PPE Exists - Do Not Work on Equipment while Energized!

## Arc Flash Notes

(*N1) Out of IEEE 1584 or NFPA 70E Ranges. LEE equation is used in this case and applicable for Open Air only. *N2) < 80\% Cleared Fault Threshold
*N3) Arcing Fault Current Low Tolerances Used
*N4) Equipment Specific Incident Energy and Flash Boundary Equations Used.
N5) Mis-coordinated, Upstream Device Tripped
(*N6) Special Instantaneous Protection in Use. Refer to Bus Detail \& Device Setting Sheets
*N7) Trip Time Unlinked with TCC.
*N8) Fault Current Unlinked with Fault Study results.
*N9) Max Arcing Duration Reached
*N10) Fuse Cable Protector Modeled.
N11) Out of IEEE 1584 Range, Lee Equation Used. Applicable for Open Air only. Existing Equipment type is not Open Air!
*N12) Out of IEEE 1584 Gap Range.
*N13) PPE up one Category
*N14) Zone Selective Interlock (ZSI) in Use.
*N15) Report as category 0 if fed by one transformer size < 125 kVA
*N16) Trip Time Recalculated
*N20) Out of NESC Voltage Range
*N21) Out of NESC Fault Current Range
N22) Out of NESC Max Clearing Range
(*N23) Out of NESC Voltage Range
*N24) Out of NESC Altitude Range
(*N25) Out of NESC Max Over Voltage Factor Range
(*N26) NESC SLG Fault is Zero

## Maximum Arc Flash Energy (US) - Danger Only

| Bus Name |  | Protective <br> Device <br> Name | Bus Volt (v) | Bus <br> Bolted Fault (kA) | Prot <br> Dev Bolted Fault (kA) | Prot <br> Dev Arcing Fault (kA) | Tripl Delay Time (sec) | Breaker Opening Time (sec) |  |  | $\begin{aligned} & 0 \\ & \frac{20}{0} \\ & 3 \\ & 3 \\ & \hline \end{aligned}$ | Arc Flash Bndry (in) | Work Dist (in) | Incident Energy (cal/cm2) | Required Protective Clothing Class |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15SWGR9001 (15SWGR9001) (315SWGR9001 MN LineSide) | 1 | 1-FDR TO 9001 | 480 | 28.65 | 28.13 | 15.82 | 2.00 | 0.000 | Y | PNL | 25 | 282 | 18 | 109.00 | Dangerous! (*N9) |
| 30SWBD9001 (30SWBD9001) (1230SWBD9001 MN LineSide) | 1 | 10-FDR TO 9002 | 480 | 30.59 | 30.51 | 17.00 | 2.00 | 0.000 | Y | PNL | 25 | 295 | 18 | 118.00 | Dangerous! (*N9) |
| 46SWGR9001 (46SWGR9001) (1846SWGR9001 MN LineSide) | 1 | 16-FDR TO 9004 | 480 | 35.43 | 35.30 | 19.25 | 2.00 | 0.000 | Y | PNL | 25 | 321 | 18 | 135.00 | Dangerous! (*N9) |

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The following general recommendations will maintain the distribution system reliability.

1. Revise, update, and redraw the Distribution System One-line drawing for the facility when new equipment is added. This will decrease trouble-shooting time, reduce errors in decision-making, and decrease engineering costs for future projects.
2. Verify that the device settings are set to the values shown in Tab 9.
3. Test and inspect all electrical equipment periodically as outlined in:
a) NFPA 70B: Electrical Equipment Maintenance
b) NETA 2009: Standard for Acceptance Testing Specifications
c) NETA 2007: Standard for Maintenance Testing Specification

TAB 3

## SHORT CIRCUIT STUDY

## Short Circuit Discussions

A short circuit study was performed to determine the available short circuit current at various locations throughout the distribution system. The following assumptions were made for the short circuit study.

1. The summary sheet in Tab 6 lists all equipment and short circuit ratings on a fully rated or series rated basis. Southern California Edison supplied the available fault current and transformer information. (3) 2500 kVA transformer with 5.75\% impedance was supplied by Southern California Edison. The available fault current used in the study is listed below.

|  |  | Available Fault Current |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Node ID\# | Node Name | Volts | 3-Phase | Line to Grd |
| 05XFMR9001S | 05XFMR9001 SEC | 480 | $37,655 \mathrm{~A}$ | $41,533 \mathrm{~A}$ |
| 05XFMR9002S | 05XFMR9002 SEC | 480 | $37,655 \mathrm{~A}$ | $41,533 \mathrm{~A}$ |
| 05XFMR9004S | 05XFMR9004 SEC | 480 | $37,647 \mathrm{~A}$ | $41,526 \mathrm{~A}$ |

2. The short circuit values calculated by the computer ignore the effect of the current limiting fuses.
3. All the motors on the MCCs without the VFDs were assumed to be operating. This assumption will produce the maximum available fault current for the distribution system.

The short circuit study was performed to verify that the existing equipment has the proper interrupting and withstand ratings. The circuit protector's (breaker, fused switch, etc.) proper application requires that the protector's short circuit current rating equal or exceed the system fault current available at the proposed protector location. However, protector short circuit ratings are based on ANSI and NEMA standards. These standards specify the test procedures used to determine the ratings. The procedures and ratings are based on time of fault initiation, asymmetrical peak, asymmetrical rms, or symmetrical rms current values.

Medium voltage circuit breakers have a momentary, also referred as close and latch, rating and interrupting rating.

1. The momentary rating is expressed as total rms current or asymmetrical rms current based on 1.6 I "d symmetrical rms at time of fault initiation.
2. The interrupting rating is expressed as symmetrical rms current for symmetrical rated breakers or total rms current for total current rated breakers either at a time of few cycles

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after fault (1.5-4 cycles). It is dependent on rated interrupting time which is a function of contact parting time including relay operating plus breaker opening time and further modified by considering the power source whether remote or local.

Medium voltage power fused and distribution cutout fuses have an interrupting or momentary rating, which are identical, expressed in symmetrical rms current or asymmetrical rms current based on 1.55 I d symmetrical rms at time of fault initiation.

The Flow Chart \#1 summarizes the method required to rate the adequacy of protective devices. There are four different categories of low voltage protectors. Each category has a different test $X / R$ ratio or power factor. The following is a summary of the categories:

Category \#1 - Low Voltage Power Circuit Breakers (without fuses) (LVPCB)
Test X/R = 6.6; P.F. = 15\%
Category \#2 - Fused Low Voltage Power Circuit Breakers, Fuses, Molded Case (MCCB) and Insulated Case (ICCB) Circuit Breakers with IAC > 20 kA.
Test $\mathrm{X} / \mathrm{R}=4.9$; P.F. $=20 \%$
Category \#3 - Molded Case (MCCB) Circuit Breakers with 10 kA < IAC < 20 kA.
Test $\mathrm{X} / \mathrm{R}=3.2$; P.F. $=30 \%$
Category \#4 - Molded Case (MCCB) Circuit Breakers with IAC < 10 kA.
Test $\mathrm{X} / \mathrm{R}=1.7$; P.F. $=50 \%$
Low voltage circuit breakers have an interrupting or momentary rating, which are identical, expressed in symmetrical rms current based on 1.01 "d symmetrical rms at time of fault initiation. However, the breakers are tested to interrupt the asymmetrical peak current at a given $X / R$ ratio or equivalent power factor.

If the fault point where the breaker is being applied has a lower power factor or higher $X / R$ ratio than the test values, then the system calculated rms symmetrical current must be modified by an X/R dependent multiplying factor (MF).

Low voltage power fuses have an interrupting or momentary rating, which are identical, expressed in symmetrical rms amperes based on 1.01 "d symmetrical rms at time of fault initiation. However, the fuses are tested to interrupt the asymmetrical peak current at a given $\mathrm{X} / \mathrm{R}$ ratio 4.899 or equivalent power factor 20 percent.

If the low voltage equipment is underrated on a fully rated basis, then the engineer applies a series rating method. If a series rating method can not be applied and the breaker is pre1982 design, then the Bussmann Up-and-Over and Up-Over-and Down Method is used. Flow chart \#2 shows this procedure and is included at the end of Tab 3.

The summary sheet in Tab 6 lists all the equipment and the short circuit ratings on a fully rated or series rated basis. There is one list for all of the devices (nodes) that are rated $>$ 600 volts. The second list is the low voltage equipment rated $<600$ volts.

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The study was performed on the existing and new equipment being installed. The calculations show that all the new equipment is properly rated for the available fault current.

## SKM PowerTools Power System Analysis Software

The short circuit study was performed using two computer programs. The main program is the SKM PowerTools program. PowerTools is a collection of programs that are used for design and analysis of power systems. The software was written and is distributed by SKM Systems Analysis Inc. of Manhattan Beach, CA.

The short circuit study required equipment nameplate data, conductor sizes, and lengths. The data were entered into PowerStudies.com's PSDB ACCESS database. This additional program stores the entire transformer, conductor, power company, and motor data.

Once the data has been entered into PSDB, the system data is imported into the SKM program. From here, short circuit, protective device, and arc flash studies can be run. The short circuit study results are exported back to PSDB where the calculated fault values are compared to the equipment short circuit ratings. A report is generated that lists the calculated short circuit current and the equipment short circuit ratings. An example of this is shown below.

## Input Data

The distribution system input data is listed at the beginning of the computer printout. The feeder, transformer, generator, utility, and motor data are listed. Following this input data is the Dapper Unbalanced Fault Report. This report lists the Bus Name, Voltage, 3 Phase fault and $X / R$ values, Single line to ground fault and $X / R$ ratios, Momentary Amps (Asymmetrical) and Asymmetrical amperes for various time periods.

For low-voltage conductors, the resistance and reactance values used in the study are based on Table 9 of the NEC. The resistance values are those at $75^{\circ} \mathrm{C}\left(167^{\circ} \mathrm{F}\right)$. Using this temperature in fault calculations is consistent with the example fault calculation carried out in ANSI/IEEE Standard 141-1986.

## Calculation of Fault Currents

The short circuit fault values were calculated using the SKM short circuit routine. The routine uses Thevennin's theorem and a bus impedance matrix to calculate the fault values. The basic calculated values fall into two forms: three phase bolted fault and line-to-ground fault values. As stated previously, the calculated short circuit current is exported from the SKM program and imported into PSDB. The PSDB program prints out a list that shows the maximum available calculated fault currents compared to the equipment short circuit rating. There is a report for Low Voltage Equipment and one for Medium Voltage. Examples of these lists are shown below.

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| Low Voltage Equipment Short Circuit Summary List |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Node ID <br> ATS-E | Node Name | Volts | Type of Device | Cat | Equip Rating |  | $\begin{gathered} \mathrm{X} / \mathrm{R} \\ \text { Ratio } \end{gathered}$ | 1/2 Cycle Sym (KA) (ACComp) | 1/2 Cycle Asym (KA) | MF | $\begin{gathered} 1 / 2 \text { Cycle } \\ \text { Sym (KA) } \\ \mathrm{X} \mathrm{MF} \\ \hline \end{gathered}$ | S\# | Type Of Fault | Equipment Underrated? |  |
|  |  |  |  |  | With | Int |  |  |  |  |  |  |  | With | Int |
|  |  | 480 |  |  |  | 42.0 | 6.23 | 0.6 | 0.7 |  |  | 2 | 3 Phase |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| ATS-N |  | 480 |  |  |  | 42.0 | 6.89 | 18.5 | 24.9 |  |  | 1 | 3 Phase |  |  |
|  |  | Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |

Table 1 - Low Voltage Short Circuit Summary List
The column descriptions are listed below:

| Field Name | Field Description |
| :--- | :--- |
| Node ID | Name of the Node, Bus, MCC, Switchgear, or Generator |
| Node Name | Longer and more description of Node ID |
| Volts | Equipment Voltage Rating |
| Type of Device | Type of Low Voltage Device <br> ATS (Automatic Transfer Switch) <br> FLVPCB (Fused Low Voltage Power Circuit Breaker) <br> FUSE |
|  | ICCB (Insulated Case Circuit Breaker) <br> LVPCB (Low Voltage Power Circuit Breaker) <br> MCCB (Molded Case Circuit Breaker) |
|  | MISC (Miscellaneous) <br> N/A (Not Applicable - No Short Circuit Rating) |
| Cat | Type of Circuit Breaker Category (See Short Circuit Device <br> Rating Procedure Flow Chart) |
| With | Withstand Rating |
| Int | Short Circuit Current Interrupting Rating (IAC) |
| X/R Ratio | Calculated X/R Ratio of maximum fault Current |
| $1 / 2$ Cycle Sym (kA) $\quad$ (AC | This is the calculated maximum $1 / 2$ Cycle Symmetrical Short <br> Circuit value |
| $1 / 2$ Cycle ASym (kA | This is the calculated maximum 1/2 Cycle Asymmetrical <br> Short Circuit value |
| MF | Multiplying Factor to increase fault current if calculated X/R <br> is greater than device test X/R ratio. (See Short Circuit <br> Device Rating Procedure Flow Chart) |
| $1 / 2$ Cycle Sym (kA) X MF | $1 / 2$ Cycle Sym (kA) current multiplied by MF (De-rates <br> device interrupting rating) Use this column and compare <br> to the equipment interrupting rating. |
| Sype of Fault | Scenario Number of the maximum fault current calculated <br> (If multiple cases are run, then there may be different case |
| or scenarios where the fault current is higher. For example |  |
| Scenario 1 - Normal Power, Scenario 2 - Emergency |  |
| Power |  |

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| Field Name | Field Description |
| :--- | :--- |
|  | properly for the available fault current. If the field is equal to <br> "Yes", then the device is underrated and has too low of a <br> withstand rating. |
| Equipment Underrated? Int | If the field is blank, then the equipment interrupting is rated <br> properly for the available fault current. If the field is equal to <br> "Yes", then the device is underrated and has too low of a <br> interrupting rating. |


| Medium Voltage Equipment Short Circuit Summary List |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Node Name | Volts | $\begin{aligned} & \text { Type } \\ & \text { of } \\ & \text { Device } \end{aligned}$ | Equip Rating <br> (KA) |  |  |  | $\begin{aligned} & \text { Int } \\ & \text { Time } \end{aligned}$ | Cont <br> Time | $\begin{gathered} \mathrm{X} / \mathrm{R} \\ \text { Ratio } \end{gathered}$ | $1 / 2$ <br> Cycle <br> Sym (KA) <br> (AC <br> Comp) | $1 / 2$ <br> Cycle <br> Asym <br> (KA) | 1@ Cont Parting Time | $\begin{gathered} \text { Calc } \\ \text { Int } \\ \text { Value } \end{gathered}$ | S\# | Type Of Fault | Equipment Underrated? |  |  |  |
| Node ID |  |  |  | $\begin{array}{\|l\|} \hline \text { Int } \\ \text { Sym } \end{array}$ | $\begin{gathered} \operatorname{Int} / \\ \mathrm{C}+\mathrm{L} \\ \text { Asym } \end{gathered}$ | With <br> Asym | $\begin{gathered} \mathrm{ST} \\ 10 \mathrm{CY} \\ \hline \end{gathered}$ |  |  |  |  |  |  |  |  |  | Int <br> Sym | $\begin{gathered} \text { Int/ } \\ \text { C+L } \\ \text { Asym } \end{gathered}$ | With <br> Asym | $\begin{gathered} \mathrm{ST} \\ 10 \mathrm{CY} \end{gathered}$ |
| PSE |  | 115000 | N/A |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| R-10 |  | 4160 | N/A |  |  |  |  |  |  | 4.49 | 18.7 | 22.9 |  |  | 1 | 3 P |  |  |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| SWGRBUS 1 |  | 4160 | PCB | 36.0 | 58.0 |  |  | 5 | 3 | 14.81 | 19.9 | 30.2 | 21.4 | 21.9 | 1 | 3 P |  |  |  |  |
|  |  | Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Table 2 - Medium Voltage Short Circuit Summary List
The column descriptions are listed below:

| Field Name | Field Description |
| :--- | :--- |
| Node ID | Name of the Node, Bus, MCC, Switchgear, or Generator |
| Node Name | Longer and more description of Node ID |
| Volts | Equipment Voltage Rating |
| Type of Device | Type of Low Voltage Device <br> FUSE <br> PCB (Medium Voltage Power Circuit Breaker) <br> MISC (Miscellaneous) <br> N/A (Not Applicable - No Short Circuit Rating) |
| Int Sym | Interrupting Short Circuit Current Rating in symmetrical <br> Amperes |
| Int/C+L Asym | Interrupting Short Circuit Current Rating in Asymmetrical <br> Amperes or Close and Latch Rating |
| With Asym | Withstand Rating in Asymmetrical Amperes |
| ST 10 CY | 10 Cycle Short Time Short Circuit Rating |
| Int Time | Nameplate Interrupting Time (Cycles) |
| Cont Part Time | Contact Parting Time |
| X/R Ratio | Calculated X/R Ratio of maximum fault Current |
| $1 / 2$ Cycle Sym (kA) <br> Comp) | This is the calculated maximum $1 / 2$ Cycle Symmetrical Short <br> Circuit value |
| $1 / 2$ Cycle ASym (kA | This is the calculated maximum 1/2 Cycle Asymmetrical <br> Short Circuit value |
| I @ Cont Parting Time | Current at contact parting time |

Tab 3 Page 6

Oxnard Advanced Water Purification
Job Number \#1104042-1
Revision \#0 - Date: 4/28/11

| Field Name | Field Description |
| :--- | :--- |
| Calc Int Value | Calculated Interrupting Value |
| S\# | Scenario Number of the maximum fault current calculated <br> (If multiple cases are run, then there may be different case <br> or scenarios where the fault current is higher. For example <br> Scenario 1 - Normal Power, Scenario 2 - Emergency <br> Power |
| Type of Fault | This lists the type of fault that produced the maximum fault <br> current. |
| Equipment Underrated? <br> Int <br> Sym | If the field is blank, then the equipment interrupting is rated <br> properly for the available fault current. If the field is equal to <br> "Yes", then the device is underrated and has too low of a <br> interrupting rating. |
| Equipment Underrated? <br> Int/ <br> C+L | If the field is blank, then the equipment interrupting is rated <br> properly for the available fault current. If the field is equal to <br> "Yes", then the device is underrated and has too low of an <br> asym |
| Equipment Underrated? <br> With <br> Asym | If the field is blank, then the equipment withstand is rated <br> properly for the available fault current. If the field is equal to |
| "Yes", then the device is underrated and has too low of a |  |
| withstand rating. |  |



Tab 3 Page 8

Oxnard Advanced Water Purification
Job Number \#1104042-1
Revision \#0 - Date: 4/28/11


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TAB 4



Note

1. PROMID FOR FUTURE IMPLEMENTATION OF AN AUTOMATIC TRANSFER
CONROLER, AND STANDBYOWER SYTEM CIRCUIT BREAKRRS AS
2. FOR ALL CONDUUT AND CONDUCTOR REQUREMENTS, SEE STTE PLAN AND

THIS DRAWING II PART OF THE ICC ANDEEECTRICAL EQUIPMENT


CH2MHILL




20MCC9101 ONE-LINE DIAGRAM



|  |  | Revisions |  | CAPTAL PROJECTS MANAGGMENT DNIIIION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\stackrel{\square}{\text { apvi }}$ |  |  |  |
|  |  |  |  | 20MCC9101 |  |  |
|  |  |  |  | nemen fucisclfen aw 7-2s-09 |  |  |
| CH2NH1LL | - |  |  |  |  |  |
| 325EASTHILCREST DRIE SUUTE 125 | Approvebeby: M VorissIs CHECKED-GY: JLHILENBRAND |  |  | $09-06 \mathrm{~A}$ | semem | 468 $\times 496$ |
| $\underset{(8055) 371-7817}{ }$ |  |  | drawn by: D CLARK <br> desicied By: M MACROSTIE | \%eme | 98-E-604 |






46SWBD9101 ONE-LINE DIAGRAM

CH2NHILL


1. FOR ALL CONDUIT AND CONDUCTOR REQUIREMENTS, SEE SITE PLAN AND
2. 200HP PUMPS WILL BE REPLACED BY 4OOHP PUMPS IN THE NEXT PHASE
3. FINAL AREAKER SIZE SHAL QEAS RECOMMENDED BY PV SYSTEM PROVIDER,

| vis |  |  | OUMAD PUBLIC WORKS |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
|  |  |  | 46SWBDI ELECCTRICAL ONE-LINE DIAGRAM |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  | ${ }^{7} 2.8009$ | $09-06 \mathrm{~A}$ | semme | $472 \times$ |
|  |  | , 7.2069 | DCCLAR | Reme | 98-E-609 |

TAB 5

DAPPER Fault Analysis Input Report (English)
Utilities

| Contribution From Name | Bus <br> Name | In/Out Service | Nominal Voltage | -------- Contribution Data ------- |  |  |  | PU (100 MVA Base |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Duty | Units | XIR |  | R PU | X PU |
| PME-5067 | 05PMS9002 | In | 16,000 | 3P: | 4,070 | Amps | 5.00 | Pos: | 0.174 | 0.869 |
|  |  |  |  | SLG: | 4,070 | Amps | 5.00 | Zero: | 0.174 | 0.869 |
| PME-7189 | 05PMS9001 | In | 16,000 | 3P: | 4,100 | Amps | 5.00 | Pos: | 0.173 | 0.863 |
|  |  |  |  | SLG: | 4,100 | Amps | 5.00 | Zero: | 0.173 | 0.863 |

Motors

| Contribution From Name | \# of <br> Motors | Bus <br> Name | In/Out Service | Nominal Voltage | --------- Contribution Data -------- |  |  | PU (100 MVA Base) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Base kVA | Xd" | X/R | R PU | X PU |
| M-20MCC9101 | 1 | 20MCC9101 | In | 480 | 97.25 | 0.2405 | 9.00 | 25.236 | 227.121 |
| M-30MCC9101 | 1 | 30MCC9101 | In | 480 | 20.18 | 0.3347 | 9.00 | 169.284 | 1,523.555 |
| M-40MCC9201 | 1 | 40MCC9201 | In | 480 | 33.54 | 0.3347 | 9.00 | 101.825 | 916.424 |
| MTR-10P1001 | 1 | 10VFD1001 | Out | 480 | 143.72 | 0.2405 | 9.00 | 0.000 | 0.000 |
| MTR-10P1002 | 1 | 10VFD1002 | Out | 480 | 143.72 | 0.2405 | 9.00 | 0.000 | 0.000 |
| MTR-10P1003 | 1 | 10VFD1003 | Out | 480 | 143.72 | 0.2405 | 9.00 | 0.000 | 0.000 |
| MTR-30P1001 | 1 | 30VFD1001 | Out | 480 | 479.07 | 0.2004 | 9.00 | 0.000 | 0.000 |
| MTR-30P1002 | 1 | 30VFD1002 | Out | 480 | 479.07 | 0.2004 | 9.00 | 0.000 | 0.000 |
| MTR-30P7600 | 1 | 30VFD7600 | Out | 480 | 143.72 | 0.2405 | 9.00 | 0.000 | 0.000 |
| MTR-30P8601 | 1 | 30VFD8601 | Out | 480 | 143.72 | 0.2405 | 9.00 | 0.000 | 0.000 |
| MTR-45P1001 | 1 | 45VFD1001 | Out | 480 | 479.07 | 0.2004 | 9.00 | 0.000 | 0.000 |
| MTR-45P1003 | 1 | 45VFD1003 | Out | 480 | 479.07 | 0.2004 | 9.00 | 0.000 | 0.000 |
| MTR-45P1006 | 1 | 45VFD1006 | Out | 480 | 191.63 | 0.2004 | 9.00 | 0.000 | 0.000 |
| MTR-45P1007 | 1 | 45VFD1007 | Out | 480 | 191.63 | 0.2004 | 9.00 | 0.000 | 0.000 |

## Cables

| Cable <br> Name | From Bus To Bus | In/Out Service | $\begin{aligned} & \text { Qty } \\ & \text { IPh } \end{aligned}$ | Length Feet | Size | ------ Cable Description ------ |  | Per Unit (100 MVA Base) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Cond. Type | Duct Type | Insul |  | R pu | jX pu |
| TO 05XFMR9001P | 05PMS9001 | In | 1 | 525 | 1-0 | Copper | Magnetic |  | Pos: | 0.0250 | 0.0114 |
|  | 05XFMR9001P |  |  |  |  |  |  |  | Zero: | 0.0382 | 0.0231 |


| Cable Name | From Bus To Bus | In/Out Service | $\begin{aligned} & \text { Qty } \\ & \text { IPh } \end{aligned}$ | Length Feet | Size | ------ Cable Description ------ |  | Per Unit ( 100 mVA Base) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Cond. Type | Duct Type | Insul |  | R pu | jX pu |
| TO 05XFMR9002P | 05PMS9001 | In | 1 | 525 | 1-0 | Copper | Magnetic |  | Pos: | 0.0250 | 0.0114 |
|  | 05XFMR9002P |  |  |  |  |  |  |  | Zero: | 0.0382 | 0.0231 |
| TO 05XFMR9004P | 05PMS9002 | In | 1 | 325 | 1-0 | Copper | Magnetic |  | Pos: | 0.0155 | 0.0070 |
|  | 05XFMR9004P |  |  |  |  |  |  |  | Zero: | 0.0237 | 0.0143 |
| TO 10DP9201 | 10SWBD9101 | In | 1 | 20 | 1-0 | Copper | Magnetic |  | Pos: | 1.0434 | 0.4774 |
|  | 10DP9201 |  |  |  |  |  |  |  | Zero: | 1.6172 | 1.1250 |
| TO 10LP9201 | 10XFMR9201S | In | 1 | 5 | 6 | Copper | Magnetic |  | Pos: | 5.6733 | 0.7396 |
|  | 10LP9201 |  |  |  |  |  |  |  | Zero: | 6.3979 | 2.0814 |
| TO 10SWBD9101 | 15SWGR9001 | In | 3 | 70 | 500 | Copper | Non-Magnetic |  | Pos: | 0.2745 | 0.3950 |
|  | 10SWBD9101 |  |  |  |  |  |  |  | Zero: | 0.9206 | 0.6451 |
| TO 10VFD1001 | 10SWBD9101 | In | 1 | 15 | 350 | Copper | Non-Magnetic |  | Pos: | 0.2474 | 0.2604 |
|  | 10VFD1001 |  |  |  |  |  |  |  | Zero: | 0.6621 | 0.4961 |
| TO 10VFD1002 | 10SWBD9101 | In | 1 | 15 | 350 | Copper | Non-Magnetic |  | Pos: | 0.2474 | 0.2604 |
|  | 10VFD1002 |  |  |  |  |  |  |  | Zero: | 0.6621 | 0.4961 |
| TO 10VFD1003 | 10SWBD9101 | In | 1 | 15 | 350 | Copper | Non-Magnetic |  | Pos: | 0.2474 | 0.2604 |
|  | 10VFD1003 |  |  |  |  |  |  |  | Zero: | 0.6621 | 0.4961 |
| TO 10XFMR9201P | 10DP9201 | In | 1 | 5 | 10 | Copper | Magnetic |  | Pos: | 2.6089 | 0.1367 |
|  | 10XFMR9201P |  |  |  |  |  |  |  | Zero: | 2.7750 | 0.4881 |
| TO 15SWGR9001 | 05XFMR9001S | In | 3 | 182 | 750 | Copper | Non-Magnetic |  | Pos: | 0.5029 | 1.0006 |
|  | 15SWGR9001 |  |  |  |  |  |  |  | Zero: | 2.1723 | 1.3876 |
| TO 20DP9201 | 20MCC9101 | In | 1 | 35 | 3 | Copper | Magnetic |  | Pos: | 3.8053 | 0.8963 |
|  | 20DP9201 |  |  |  |  |  |  |  | Zero: | 4.6955 | 2.3409 |
| TO 20LP9201 | 20XFMR9201S | In | 1 | 5 | 6 | Copper | Magnetic |  | Pos: | 5.6733 | 0.7396 |
|  | 20LP9201 |  |  |  |  |  |  |  | Zero: | 6.3979 | 2.0814 |
| TO 20MCC9101 | 15SWGR9001 | In | 2 | 50 | 350 | Copper | Non-Magnetic |  | Pos: | 0.4123 | 0.4340 |
|  | 20MCC9101 |  |  |  |  |  |  |  | Zero: | 1.1035 | 0.8268 |
| TO 20XFMR9201P | 20DP9201 | In | 1 | 5 | 10 | Copper | Magnetic |  | Pos: | 2.6089 | 0.1367 |
|  | 20XFMR9201P |  |  |  |  |  |  |  | Zero: | 2.7750 | 0.4881 |
| TO 30DP9201 | 30SWBD9001 | In | 1 | 110 | 1-0 | Copper | Magnetic |  | Pos: | 5.7387 | 2.6259 |
|  | 30DP9201 |  |  |  |  |  |  |  | Zero: | 8.8945 | 6.1875 |
| TO 30LP9201 | 30XFMR9201S | In | 1 | 5 | 6 | Copper | Magnetic |  | Pos: | 5.6733 | 0.7396 |
|  | 30LP9201 |  |  |  |  |  |  |  | Zero: | 6.3979 | 2.0814 |
| TO 30MCC9101 | 30SWBD9001 | In | 1 | 20 | 1-0 | Copper | Non-Magnetic |  | Pos: | 1.0434 | 0.3819 |
|  | 30MCC9101 |  |  |  |  |  |  |  | Zero: | 1.6172 | 0.9375 |
| TO 30MTS8601 | 30SWBD9001 | In | 1 | 15 | 300 | Copper | Non-Magnetic |  | Pos: | 0.2871 | 0.2669 |
|  | 30MTS8601 |  |  |  |  |  |  |  | Zero: | 0.7018 | 0.5339 |
| TO 30SWBD9001 | 05XFMR9002S | In | 4 | 169 | 750 | Copper | Non-Magnetic |  | Pos: | 0.3502 | 0.6968 |
|  | 30SWBD9001 |  |  |  |  |  |  |  | Zero: | 1.5129 | 0.9664 |
| TO 30VFD1001 | 30SWBD9001 | In | 3 | 26 | 500 | Copper | Non-Magnetic |  | Pos: | 0.1019 | 0.1467 |
|  | 30VFD1001 |  |  |  |  |  |  |  | Zero: | 0.3419 | 0.2396 |
| TO 30VFD1002 | 30SWBD9001 | In | 3 | 26 | 500 | Copper | Non-Magnetic |  | Pos: | 0.1019 | 0.1467 |
|  | 30VFD1002 |  |  |  |  |  |  |  | Zero: | 0.3419 | 0.2396 |


| Cable Name | From Bus To Bus | In/Out Service | $\begin{aligned} & \text { Qty } \\ & \text { IPh } \end{aligned}$ | Length Feet | Size | ------ Cable Description ------ |  | Per Unit ( $\mathbf{1 0 0}$ MVA Base) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Cond. Type | Duct Type | Insul |  | R pu | jX pu |
| TO 30VFD7600 | 30SWBD9001 | In | 1 | 15 | 300 | Copper | Non-Magnetic |  | Pos: | 0.2871 | 0.2669 |
|  | 30VFD7600 |  |  |  |  |  |  |  | Zero: | 0.7018 | 0.5339 |
| TO 30VFD8601 | 30MTS8601 | In | 1 | 20 | 300 | Copper | Non-Magnetic |  |  | 0.3828 | 0.3559 |
|  | 30VFD8601 |  |  |  |  |  |  |  | Zero: | 0.9358 | 0.7118 |
| TO 30XFMR9201P | 30DP9201 | In | 1 | 5 | 10 | Copper | Magnetic |  |  | 2.6089 | 0.1367 |
|  | 30XFMR9201P |  |  |  |  |  |  |  | Zero: | 2.7750 | 0.4881 |
| TO 40DP9201 | 46SWBD9101 | In | 1 | 25 | 1-0 | Copper | Magnetic |  |  | 1.3043 | 0.5968 |
|  | 40DP9201 |  |  |  |  |  |  |  | Zero: | 2.0215 | 1.4063 |
| TO 40DP9202 | 46SWBD9101 | In | 1 | 140 | 1-0 | Copper | Magnetic |  | Pos: | 7.3038 | 3.3420 |
|  | 40DP9202 |  |  |  |  |  |  |  | Zero: | 11.3203 | 7.8750 |
| TO 40LP9201 | 40XFMR9201S | In | 1 | 5 | 6 | Copper | Magnetic |  | Pos: | 5.6733 | 0.7396 |
|  | 40LP9201 |  |  |  |  |  |  |  | Zero: | 6.3979 | 2.0814 |
| TO 40LP9202 | 40XFMR9202S | In | 1 | 5 | 6 | Copper | Magnetic |  | Pos: | 5.6733 | 0.7396 |
|  | 40LP9202 |  |  |  |  |  |  |  | Zero: | 6.3979 | 2.0814 |
| TO 40MCC9201 | 40SWBD9101 | In | 1 | 35 | 2 | Copper | Non-Magnetic |  | Pos: | 2.8924 | 0.6836 |
|  | 40MCC9201 |  |  |  |  |  |  |  | Zero: | 3.9178 | 1.8427 |
| TO 40SWBD9101 | 46SWGR9001 | In | 2 | 20 | 350 | Copper | Non-Magnetic |  | Pos: | 0.1649 | 0.1736 |
|  | 40SWBD9101 |  |  |  |  |  |  |  | Zero: | 0.4414 | 0.3307 |
| TO 40XFMR9201P | 40DP9201 | In | 1 | 5 | 10 | Copper | Magnetic |  | Pos: | 2.6089 | 0.1367 |
|  | 40XFMR9201P |  |  |  |  |  |  |  | Zero: | 2.7750 | 0.4881 |
| TO 40XFMR9202P | 40DP9202 | In | 1 | 5 | 10 | Copper | Magnetic |  | Pos: | 2.6089 | 0.1367 |
|  | 40XFMR9202P |  |  |  |  |  |  |  | Zero: | 2.7750 | 0.4881 |
| TO 45VFD1001 | 46SWBD9101 | In | 3 | 30 | 500 | Copper | Non-Magnetic |  | Pos: | 0.1176 | 0.1693 |
|  | 45VFD1001 |  |  |  |  |  |  |  | Zero: | 0.3945 | 0.2765 |
| TO 45VFD1003 | 46SWBD9101 | In | 3 | 30 | 500 | Copper | Non-Magnetic |  | Pos: | 0.1176 | 0.1693 |
|  | 45VFD1003 |  |  |  |  |  |  |  | Zero: | 0.3945 | 0.2765 |
| TO 45VFD1006 | 46SWBD9101 | In | 1 | 50 | 500 | Copper | Non-Magnetic |  | Pos: | 0.5881 | 0.8464 |
|  | 45VFD1006 |  |  |  |  |  |  |  | Zero: | 1.9727 | 1.3824 |
| TO 45VFD1007 | 46SWBD9101 | In | 1 | 60 | 500 | Copper | Non-Magnetic |  | Pos: | 0.7057 | 1.0156 |
|  | 45VFD1007 |  |  |  |  |  |  |  | Zero: | 2.3672 | 1.6589 |
| TO 46SWBD9101 | 46SWGR9001 | In | 5 | 45 | 600 | Copper | Non-Magnetic |  | Pos: | 0.0898 | 0.1523 |
|  | 46SWBD9101 |  |  |  |  |  |  |  | Zero: | 0.3387 | 0.2367 |
| TO 46SWGR9001 | 05XFMR9004S | In | 5 | 60 | 750 | Copper | Non-Magnetic |  | Pos: | 0.0995 | 0.1979 |
|  | 46SWGR9001 |  |  |  |  |  |  |  | Zero: | 0.4297 | 0.2745 |
| TO 50DP9201 | 46SWBD9101 | In | 1 | 240 | 4-0 | Copper | Magnetic |  | Pos: | 6.5729 | 5.3125 |
|  | 50DP9201 |  |  |  |  |  |  |  | Zero: | 13.0625 | 11.3229 |
| TO 50LP9201 | 50XFMR9201S | In | 1 | 5 | 1 | Copper | Magnetic |  | Pos: | 1.8526 | 0.6587 |
|  | 50LP9201 |  |  |  |  |  |  |  | Zero: | 2.5252 | 1.6029 |
| TO 50LP9202 | 50LP9201 | In | 1 | 15 | 1 | Copper | Magnetic |  | Pos: | 5.5577 | 1.9762 |
|  | 50LP9202 |  |  |  |  |  |  |  | Zero: | 7.5756 | 4.8088 |
| TO 50XFMR9201P | 50DP9201 | In | 1 | 5 | 6 | Copper | Magnetic |  | Pos: | 1.0653 | 0.1389 |
|  | 50XFMR9201P |  |  |  |  |  |  |  | Zero: | 1.2014 | 0.3908 |


| Cable <br> Name | From Bus To Bus | In/Out Service | QtyIPh | Length Feet | Size | ------ Cable Description ------ |  | Per Unit (100 MVA Base) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Cond. Type | Duct Type | Insul |  | R pu | jX pu |
| TO 70DP9201 | 10SWBD9101 <br> 70DP9201 | In | 1 | 320 | 4-0 | Copper | Magnetic |  | $\begin{array}{r} \hline \text { Pos: } \\ \text { Zero: } \end{array}$ | $\begin{array}{r} 8.7639 \\ 17.4167 \end{array}$ | $\begin{array}{r} 7.0833 \\ 15.0972 \end{array}$ |
| TO 70LP9201 | 70XFMR9201S <br> 70LP9201 | In | 1 | 5 | 1 | Copper | Magnetic |  | $\begin{gathered} \text { Pos: } \\ \text { Zero: } \end{gathered}$ | $\begin{aligned} & 1.8526 \\ & 2.5252 \end{aligned}$ | $\begin{aligned} & 0.6587 \\ & 1.6029 \end{aligned}$ |
| TO 70LP9202 | $\begin{aligned} & \text { 70XFMR9202S } \\ & \text { 70LP9202 } \end{aligned}$ | In | 1 | 5 | 1 | Copper | Magnetic |  | $\begin{gathered} \text { Pos: } \\ \text { Zero: } \end{gathered}$ | $\begin{aligned} & 1.8526 \\ & 2.5252 \end{aligned}$ | $\begin{aligned} & 0.6587 \\ & 1.6029 \end{aligned}$ |
| TO 70XFMR9201P | $\begin{aligned} & \text { 70DP9201 } \\ & \text { 70XFMR9201P } \end{aligned}$ | In | 1 | 5 | 6 | Copper | Magnetic |  | $\begin{gathered} \text { Pos: } \\ \text { Zero: } \end{gathered}$ | $\begin{aligned} & 1.0653 \\ & 1.2014 \end{aligned}$ | $\begin{aligned} & 0.1389 \\ & 0.3908 \end{aligned}$ |
| TO 70XFMR9202P | $\begin{aligned} & \text { 70DP9201 } \\ & \text { 70XFMR9202P } \end{aligned}$ | In | 1 | 5 | 6 | Copper | Magnetic |  | $\begin{gathered} \text { Pos: } \\ \text { Zero: } \end{gathered}$ | $\begin{aligned} & 1.0653 \\ & 1.2014 \end{aligned}$ | $\begin{aligned} & 0.1389 \\ & 0.3908 \end{aligned}$ |

## 2-Winding Transformers

| Xformer Name | In/Out Service | ----------------Pי-Primary \& Secondary------------- |  |  |  | Nominal kVA | Z PU (100 MVA Base) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Bus | Conn. | Volts | FLA |  |  | R pu | jX pu |
| 05XFMR9001 | In | 05XFMR9001P | D | 16,000 | 90 | 2,500.0 | Pos: | 0.3247 | 2.2770 |
|  |  | 05XFMR9001S | WG | 480 | 3,007 |  | Zero: | 0.3247 | 2.2770 |
| 05XFMR9002 | In | 05XFMR9002P | D | 16,000 | 90 | 2,500.0 | Pos: | 0.3247 | 2.2770 |
|  |  | 05XFMR9002S | WG | 480 | 3,007 |  | Zero: | 0.3247 | 2.2770 |
| 05XFMR9004 | In | 05XFMR9004P | D | 16,000 | 90 | 2,500.0 | Pos: | 0.3247 | 2.2770 |
|  |  | 05XFMR9004S | WG | 480 | 3,007 |  | Zero: | 0.3247 | 2.2770 |
| 10XFMR9201 | In | 10XFMR9201P | D | 480 | 18 | 15.0 | Pos: | 206.6667 | 153.3333 |
|  |  | 10XFMR9201S | WG | 208 | 42 |  | Zero: | 206.6667 | 153.3333 |
| 20XFMR9201 | In | 20XFMR9201P | D | 480 | 18 | 15.0 | Pos: | 206.6667 | 153.3333 |
|  |  | 20XFMR9201S | WG | 208 | 42 |  | Zero: | 206.6667 | 153.3333 |
| 30XFMR9201 | In | 30XFMR9201P | D | 480 | 18 | 15.0 | Pos: | 206.6667 | 153.3333 |
|  |  | 30XFMR9201S | WG | 208 | 42 |  | Zero: | 206.6667 | 153.3333 |
| 40XFMR9201 | In | 40XFMR9201P | D | 480 | 18 | 15.0 | Pos: | 206.6667 | 153.3333 |
|  |  | 40XFMR9201S | WG | 208 | 42 |  | Zero: | 206.6667 | 153.3333 |
| 40XFMR9202 | In | 40XFMR9202P | D | 480 | 18 | 15.0 | Pos: | 206.6667 | 153.3333 |
|  |  | 40XFMR9202S | WG | 208 | 42 |  | Zero: | 206.6667 | 153.3333 |
| 50XFMR9201 | In | 50XFMR9201P | D | 480 | 36 | 30.0 | Pos: | 103.3333 | 76.6667 |
|  |  | 50XFMR9201S | WG | 208 | 83 |  | Zero: | 103.3333 | 76.6667 |
| 70XFMR9201 | In | 70XFMR9201P | D | 480 | 36 | 30.0 | Pos: | 103.3333 | 76.6667 |
|  |  | 70XFMR9201S | WG | 208 | 83 |  | Zero: | 103.3333 | 76.6667 |
| 70XFMR9202 | In | 70XFMR9202P | D | 480 | 36 | 30.0 | Pos: | 103.3333 | 76.6667 |
|  |  | 70XFMR9202S | WG | 208 | 83 |  | Zero: | 103.3333 | 76.6667 |

## Project: 1104042-1

DAPPER Unbalanced Fault Report

Comprehensive Short Circuit Study Settings

| Three Phase Fault | Yes |  |  |  | Faulted Bus |  | All Buses |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Single Line to Ground | Yes |  |  |  | Bus Voltages |  | First Bus From Fault |  |  |  |  |
| Line to Line Fault | No |  |  |  | Branch Currents |  | First Branch From Fault |  |  |  |  |
| Line to Line to Ground | No |  |  |  | Phase or Sequence |  | Report phase quantities |  |  |  |  |
| Motor Contribution | Yes |  |  |  | Fault Current Calculation |  | Asymmetrical RMS (with DC offset and Decay) |  |  |  |  |
| Transformer Tap | Yes |  |  |  | Asym Fault Current at Time |  | 4.00 | Cycles |  |  |  |
| Xformer Phase Shift | Yes |  |  |  |  |  |  |  |  |  |  |
| Fault Location Bus Name | Bus Voltage | 3-Phase Amps | 3-Phase MVA | $\begin{array}{r} 3 P \\ \text { X/R } \end{array}$ | $\begin{array}{r} \text { SLG } \\ \text { Amps } \end{array}$ | $\begin{aligned} & \text { SLG } \\ & \text { MVA } \end{aligned}$ | $\begin{gathered} \text { SLG } \\ \text { XIR } \end{gathered}$ | Mom <br> Amps | ---------3P Asym Amps-------- |  |  |
|  |  |  |  |  |  |  |  |  | 3 Cycles | 5 Cycles | 8 Cycles |
| 05PMS9001 | 16,000 | 4,118 | 114.12 | 5.01 | 4,112 | 37.98 | 5.01 | 5,161 | 4,120 | 4,118 | 4,118 |
| 05PMS9002 | 16,000 | 4,074 | 112.90 | 5.00 | 4,073 | 37.62 | 5.00 | 5,104 | 4,076 | 4,074 | 4,074 |
| 05XFMR9001P | 16,000 | 4,043 | 112.05 | 4.44 | 4,016 | 37.09 | 4.35 | 4,927 | 4,044 | 4,043 | 4,043 |
| 05XFMR9001S | 480 | 38,183 | 31.74 | 6.06 | 42,070 | 11.66 | 6.29 | 49,919 | 38,259 | 38,184 | 38,183 |
| 05XFMR9002P | 16,000 | 4,043 | 112.03 | 4.43 | 4,015 | 37.09 | 4.35 | 4,926 | 4,043 | 4,043 | 4,043 |
| 05XFMR9002S | 480 | 37,772 | 31.40 | 6.04 | 41,644 | 11.54 | 6.27 | 49,350 | 37,846 | 37,773 | 37,772 |
| 05XFMR9004P | 16,000 | 4,028 | 111.64 | 4.63 | 4,014 | 37.08 | 4.58 | 4,958 | 4,030 | 4,028 | 4,028 |
| 05XFMR9004S | 480 | 37,777 | 31.41 | 6.14 | 41,659 | 11.54 | 6.35 | 49,528 | 37,858 | 37,778 | 37,777 |
| 10DP9201 | 480 | 22,009 | 18.30 | 2.14 | 19,987 | 5.54 | 1.59 | 23,146 | 22,009 | 22,009 | 22,009 |
| 10LP9201 | 208 | 1,031 | 0.37 | 0.73 | 1,038 | 0.12 | 0.73 | 1,031 | 1,031 | 1,031 | 1,031 |
|  |  |  |  |  | 1 |  |  |  |  |  |  |


| Fault Location Bus Name | Bus <br> Voltage | 3-Phase Amps | 3-Phase MVA | $\begin{array}{r} 3 P \\ X / R \end{array}$ | $\begin{array}{r} \text { SLG } \\ \text { Amps } \end{array}$ | $\begin{aligned} & \text { SLG } \\ & \text { MVA } \end{aligned}$ | $\begin{gathered} \text { SLG } \\ \text { X/R } \end{gathered}$ | Mom Amps | ---------3P Asym Amps-------- |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  | 3 Cycles | 5 Cycles | 8 Cycles |
| 10SWBD9101 | 480 | 25,865 | 21.50 | 3.52 | 24,942 | 6.91 | 2.25 | 29,889 | 25,865 | 25,865 | 25,865 |
| 10VFD1001 | 480 | 24,195 | 20.12 | 3.12 | 22,723 | 6.30 | 2.02 | 27,228 | 24,195 | 24,195 | 24,195 |
| 10VFD1002 | 480 | 24,195 | 20.12 | 3.12 | 22,723 | 6.30 | 2.02 | 27,228 | 24,195 | 24,195 | 24,195 |
| 10VFD1003 | 480 | 24,195 | 20.12 | 3.12 | 22,723 | 6.30 | 2.02 | 27,228 | 24,195 | 24,195 | 24,195 |
| 10XFMR9201P | 480 | 16,989 | 14.12 | 1.03 | 15,154 | 4.20 | 0.91 | 17,028 | 16,989 | 16,989 | 16,989 |
| 10XFMR9201S | 208 | 1,050 | 0.38 | 0.75 | 1,059 | 0.13 | 0.75 | 1,050 | 1,050 | 1,050 | 1,050 |
| 15SWGR9001 | 480 | 28,650 | 23.82 | 4.09 | 28,680 | 7.95 | 2.67 | 34,268 | 28,652 | 28,650 | 28,650 |
| 20DP9201 | 480 | 16,059 | 13.35 | 1.04 | 14,120 | 3.91 | 0.95 | 16,097 | 16,059 | 16,059 | 16,059 |
| 20LP9201 | 208 | 1,021 | 0.37 | 0.72 | 1,031 | 0.12 | 0.73 | 1,021 | 1,021 | 1,021 | 1,021 |
| 20MCC9101 | 480 | 25,547 | 21.24 | 3.23 | 24,346 | 6.75 | 2.15 | 28,979 | 25,547 | 25,547 | 25,547 |
| 20XFMR9201P | 480 | 12,574 | 10.45 | 0.71 | 11,184 | 3.10 | 0.69 | 12,576 | 12,574 | 12,574 | 12,574 |
| 20XFMR9201S | 208 | 1,040 | 0.37 | 0.74 | 1,053 | 0.13 | 0.74 | 1,040 | 1,040 | 1,040 | 1,040 |
| 30DP9201 | 480 | 13,016 | 10.82 | 0.98 | 11,018 | 3.05 | 0.93 | 13,037 | 13,016 | 13,016 | 13,016 |
| 30LP9201 | 208 | 1,014 | 0.37 | 0.73 | 1,027 | 0.12 | 0.73 | 1,014 | 1,014 | 1,014 | 1,014 |
| 30MCC9101 | 480 | 25,995 | 21.61 | 2.21 | 24,812 | 6.88 | 1.74 | 27,472 | 25,995 | 25,995 | 25,995 |
| 30MTS8601 | 480 | 28,222 | 23.46 | 3.55 | 27,932 | 7.74 | 2.47 | 32,679 | 28,223 | 28,222 | 28,222 |
| 30SWBD9001 | 480 | 30,587 | 25.43 | 4.42 | 31,440 | 8.71 | 3.06 | 37,238 | 30,593 | 30,587 | 30,587 |
| 30VFD1001 | 480 | 29,347 | 24.40 | 4.10 | 29,678 | 8.22 | 2.78 | 35,127 | 29,350 | 29,347 | 29,347 |
| 30VFD1002 | 480 | 29,347 | 24.40 | 4.10 | 29,678 | 8.22 | 2.78 | 35,127 | 29,350 | 29,347 | 29,347 |
| 30VFD7600 | 480 | 28,222 | 23.46 | 3.55 | 27,932 | 7.74 | 2.47 | 32,679 | 28,223 | 28,222 | 28,222 |
| 30VFD8601 | 480 | 25,504 | 21.20 | 2.90 | 24,197 | 6.71 | 2.05 | 28,272 | 25,504 | 25,504 | 25,504 |
| 30XFMR9201P | 480 | 10,612 | 8.82 | 0.72 | 9,155 | 2.54 | 0.72 | 10,614 | 10,612 | 10,612 | 10,612 |
| 30XFMR9201S | 208 | 1,033 | 0.37 | 0.74 | 1,048 | 0.13 | 0.74 | 1,033 | 1,033 | 1,033 | 1,033 |
| 40DP9201 | 480 | 26,417 | 21.96 | 2.04 | 25,291 | 7.01 | 1.74 | 27,603 | 26,417 | 26,417 | 26,417 |
| 40DP9202 | 480 | 11,429 | 9.50 | 0.85 | 9,647 | 2.67 | 0.86 | 11,436 | 11,429 | 11,429 | 11,429 |
| 40LP9201 | 208 | 1,034 | 0.37 | 0.73 | 1,040 | 0.12 | 0.73 | 1,034 | 1,034 | 1,034 | 1,034 |
| 40LP9202 | 208 | 1,009 | 0.36 | 0.72 | 1,023 | 0.12 | 0.72 | 1,009 | 1,009 | 1,009 | 1,009 |


| Fault Location Bus Name | Bus Voltage | 3-Phase Amps | 3-Phase <br> MVA | $\begin{array}{r} 3 P \\ \times I R \end{array}$ | $\begin{array}{r} \text { SLG } \\ \text { Amps } \end{array}$ | SLG <br> MVA | $\begin{gathered} \text { SLG } \\ \text { X/R } \end{gathered}$ | Mom Amps | ---------3P Asym Amps-------- |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  | 3 Cycles | 5 Cycles | 8 Cycles |
| 40MCC9201 | 480 | 21,646 | 18.00 | 1.15 | 20,033 | 5.55 | 1.06 | 21,739 | 21,646 | 21,646 | 21,646 |
| 40SWBD9101 | 480 | 33,450 | 27.81 | 4.54 | 35,140 | 9.74 | 3.62 | 40,977 | 33,458 | 33,450 | 33,450 |
| 40XFMR9201P | 480 | 19,227 | 15.99 | 0.92 | 18,027 | 5.00 | 0.87 | 19,247 | 19,227 | 19,227 | 19,227 |
| 40XFMR9201S | 208 | 1,053 | 0.38 | 0.75 | 1,062 | 0.13 | 0.74 | 1,053 | 1,053 | 1,053 | 1,053 |
| 40XFMR9202P | 480 | 9,473 | 7.88 | 0.66 | 8,161 | 2.26 | 0.69 | 9,474 | 9,473 | 9,473 | 9,473 |
| 40XFMR9202S | 208 | 1,028 | 0.37 | 0.74 | 1,044 | 0.13 | 0.74 | 1,028 | 1,028 | 1,028 | 1,028 |
| 45VFD1001 | 480 | 32,066 | 26.66 | 4.48 | 33,294 | 9.23 | 3.33 | 39,159 | 32,073 | 32,066 | 32,066 |
| 45VFD1003 | 480 | 32,066 | 26.66 | 4.48 | 33,294 | 9.23 | 3.33 | 39,159 | 32,073 | 32,066 | 32,066 |
| 45VFD1006 | 480 | 26,581 | 22.10 | 3.37 | 25,732 | 7.13 | 2.28 | 30,416 | 26,581 | 26,581 | 26,581 |
| 45VFD1007 | 480 | 25,476 | 21.18 | 3.21 | 24,310 | 6.74 | 2.15 | 28,842 | 25,476 | 25,476 | 25,476 |
| 46SWBD9101 | 480 | 33,777 | 28.08 | 4.99 | 35,809 | 9.92 | 3.92 | 42,285 | 33,795 | 33,777 | 33,777 |
| 46SWGR9001 | 480 | 35,434 | 29.46 | 5.47 | 38,260 | 10.60 | 4.68 | 45,297 | 35,470 | 35,435 | 35,434 |
| 50DP9201 | 480 | 10,533 | 8.76 | 1.21 | 8,437 | 2.34 | 1.11 | 10,591 | 10,533 | 10,533 | 10,533 |
| 50LP9201 | 208 | 1,947 | 0.70 | 0.76 | 1,998 | 0.24 | 0.75 | 1,947 | 1,947 | 1,947 | 1,947 |
| 50LP9202 | 208 | 1,873 | 0.67 | 0.74 | 1,905 | 0.23 | 0.74 | 1,873 | 1,873 | 1,873 | 1,873 |
| 50XFMR9201P | 480 | 9,837 | 8.18 | 1.07 | 7,923 | 2.20 | 1.01 | 9,865 | 9,837 | 9,837 | 9,837 |
| 50XFMR9201S | 208 | 1,973 | 0.71 | 0.77 | 2,031 | 0.24 | 0.76 | 1,973 | 1,973 | 1,973 | 1,973 |
| $70 \mathrm{DP9} 201$ | 480 | 7,859 | 6.53 | 1.15 | 6,124 | 1.70 | 1.04 | 7,892 | 7,859 | 7,859 | 7,859 |
| 70LP9201 | 208 | 1,895 | 0.68 | 0.77 | 1,961 | 0.24 | 0.76 | 1,896 | 1,895 | 1,895 | 1,895 |
| 70LP9202 | 208 | 1,895 | 0.68 | 0.77 | 1,961 | 0.24 | 0.76 | 1,896 | 1,895 | 1,895 | 1,895 |
| 70XFMR9201P | 480 | 7,459 | 6.20 | 1.05 | 5,844 | 1.62 | 0.98 | 7,479 | 7,459 | 7,459 | 7,459 |
| 70XFMR9201S | 208 | 1,920 | 0.69 | 0.77 | 1,993 | 0.24 | 0.76 | 1,920 | 1,920 | 1,920 | 1,920 |
| 70XFMR9202P | 480 | 7,459 | 6.20 | 1.05 | 5,844 | 1.62 | 0.98 | 7,479 | 7,459 | 7,459 | 7,459 |
| 70XFMR9202S | 208 | 1,920 | 0.69 | 0.77 | 1,993 | 0.24 | 0.76 | 1,920 | 1,920 | 1,920 | 1,920 |

TAB 6

## Medium Voltage Equipment Short Circuit Summary List

| Node ID | Node Name | Volts | Type of Device | Equip Rating (KA) |  |  |  | Int Time | Cont Part <br> Time | $\begin{gathered} \text { XIR } \\ \text { Ratio } \end{gathered}$ | $1 / 2$ <br> Cycle <br> Sym(KA) <br> (AC <br> Comp) | 1/2 <br> Cycle <br> Asym <br> (KA) | I @ Cont Parting Time | $\begin{gathered} \text { Calc } \\ \text { Int } \\ \text { Value } \end{gathered}$ | S\# | Type Of <br> Fault | Equipment Underrated? |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Int <br> Sym | Int/ C+L Asym | With Asym |  |  |  |  |  |  |  |  |  |  | Int <br> Sym | $\begin{array}{\|c\|} \hline \text { Int/ } \\ \text { C+L } \\ \text { Asym } \\ \hline \end{array}$ | With <br> Asym | $\begin{gathered} \text { ST } \\ 10 \mathrm{CY} \end{gathered}$ |
| 05PMS9001 | 05PMS9001 | 16000 | FUSE | 12.5 |  | 20.0 |  |  |  | 5.01 | 4.1 | 5.2 |  |  | 1 | 3 P |  |  |  |  |
| Comment: Ratings Based On Fuse, Utility's Responsibility. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 05PMS9002 | 05PMS9002 | 16000 | FUSE | 12.5 |  | 20.0 |  |  |  | 5.00 | 4.1 | 5.1 |  |  | 1 | 3 P |  |  |  |  |
| Comment: Ratings Based On Fuse, Utility's Responsibility. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 05XFMR9001 | 05XFMR9001 PRI | 16000 | N/A |  |  |  |  |  |  | 4.44 | 4.0 | 4.9 |  |  | 1 | 3 P |  |  |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 05XFMR9002 | 05XFMR9002 PRI | 16000 | N/A |  |  |  |  |  |  | 4.43 | 4.0 | 4.9 |  |  | 1 | 3 P |  |  |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 05XFMR9004 | 05XFMR9004 PRI | 16000 | N/A |  |  |  |  |  |  | 4.63 | 4.0 | 5.0 |  |  | 1 | 3 P |  |  |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| PME-5067 | PME 5067 | 16000 | N/A |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| PME-7189 | PME 7189 | 16000 | N/A |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| Low Voltage Equipment Short circuit Summary List |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Node ID | Node Name | Volts | Type of Device | Cat | Equip Rating |  | XIR <br> Ratio | 1/2 Cycle Sym (KA) <br> (ACComp) | 1/2 Cycle Asym (KA) | MF | 1/2 Cycle <br> Sym (KA) <br> X MF | S\# | Type Of Fault | Equipment Underrated? |  |
|  |  |  |  |  | With | Int |  |  |  |  |  |  |  | With | Int |
| 05XFMR9001 | 05XFMR9001 SEC | 480 | N/A |  |  |  | 6.29 | 42.1 | 55.4 |  |  | 1 | Line To Ground |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 05XFMR900205XFMR9002 SEC |  | 480 | N/A |  |  |  | 6.27 | 41.6 | 54.8 |  |  | 1 | Line To Ground |  |  |
|  |  | Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 05XFMR9004 05XFMR9004 SEC |  | 480 | N/A |  |  |  | 6.35 | 41.7 | 55.0 |  |  | 1 | Line To Ground |  |  |
|  |  | Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10DP9201 | 10DP9201 | 480 | MCCB | 2 |  | 35.0 | 2.14 | 22.0 | 23.1 | 1 | 22.0 | 1 | 3 Phase |  |  |
|  |  | Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10LP9201 | 10LP9201 | 208 | MCCB | 4 |  | 10.0 | 0.73 | 1.0 | 1.0 | 1 | 1.0 | 1 | Line To Ground |  |  |
|  |  | Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $10 S W B D 910$ $10 S W B D 9101$ |  | 480 | MCCB | 2 |  | 50.0 | 3.52 | 25.9 | 29.9 | 1 | 25.9 | 1 | 3 Phase |  |  |
|  |  | Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10VFD1001 | 10VFD1001 | 480 | MCCB | 2 |  | 65.0 | 3.12 | 24.2 | 27.2 | 1 | 24.2 | 1 | 3 Phase |  |  |
|  |  | Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10VFD1002 | 10VFD1002 | 480 | MCCB | 2 |  | 65.0 | 3.12 | 24.2 | 27.2 | 1 | 24.2 | 1 | 3 Phase |  |  |
|  |  | Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10VFD1003 | 10VFD1003 | 480 | MCCB | 2 |  | 65.0 | 3.12 | 24.2 | 27.2 | 1 | 24.2 | 1 | 3 Phase |  |  |
|  |  | Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10XFMR9201 10XFMR9201 PRI |  | 480 | N/A |  |  |  | 1.03 | 17.0 | 17.0 |  |  | 1 | 3 Phase |  |  |
|  |  | Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Low Voltage Equipment Short Circuit Summary List



## Low Voltage Equipment Short Circuit Summary List

| Node ID | Node Name | Volts | Type of Device | Cat | Equip Rating |  | XIR <br> Ratio | 1/2 Cycle Sym (KA) (ACComp) | 1/2 Cycle Asym (KA) | MF | 1/2 Cycle <br> Sym (KA) <br> X MF | S\# | Type Of Fault | Equipment Underrated? |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | With | Int |  |  |  |  |  |  |  | With | Int |
| 30SWBD900 | 30SWBD9001 | 480 | MCCB | 2 |  | 50.0 | 4.42 | 30.6 | 37.2 | 1 | 30.6 | 1 | 3 Phase |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30VFD1001 | 30VFD1001 | 480 | MCCB | 2 |  | 50.0 | 4.10 | 29.3 | 35.1 | 1 | 29.3 | 1 | 3 Phase |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30VFD1002 | 30VFD1002 | 480 | MCCB | 2 |  | 50.0 | 4.10 | 29.3 | 35.1 | 1 | 29.3 | 1 | 3 Phase |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30VFD7600 | 30VFD7600 | 480 | MCCB | 2 |  | 65.0 | 3.55 | 28.2 | 32.7 | 1 | 28.2 | 1 | 3 Phase |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30VFD8601 | 30VFD8601 | 480 | MCCB | 2 |  | 65.0 | 2.90 | 25.5 | 28.3 | 1 | 25.5 | 1 | 3 Phase |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30XFMR9201 | 30XFMR9201 PRI | 480 | N/A |  |  |  | 0.72 | 10.6 | 10.6 |  |  | 1 | 3 Phase |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30XFMR9201 | 30XFMR9201 SEC | 208 | N/A |  |  |  | 0.74 | 1.0 | 1.0 |  |  | 1 | Line To Ground |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 40DP9201 | 40DP9201 | 480 | MCCB | 2 |  | 35.0 | 2.04 | 26.4 | 27.6 | 1 | 26.4 | 1 | 3 Phase |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 40DP9202 | 40DP9202 | 480 | MCCB | 2 |  | 35.0 | 0.85 | 11.4 | 11.4 | 1 | 11.4 | 1 | 3 Phase |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 40LP9201 | 40LP9201 | 208 | MCCB | 4 |  | 10.0 | 0.73 | 1.0 | 1.0 | 1 | 1.0 | 1 | Line To Ground |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 40LP9202 | 40LP9202 | 208 | MCCB | 4 |  | 10.0 | 0.72 | 1.0 | 1.0 | 1 | 1.0 | 1 | Line To Ground |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Low Voltage Equipment Short Circuit Summary List

| Node Name | Volts | Type of Device | Cat | Equip Rating |  | XIR <br> Ratio | 1/2 Cycle Sym (KA) (ACComp) | 1/2 Cycle Asym (KA) | MF | 1/2 Cycle <br> Sym (KA) <br> X MF | S\# | Type Of Fault | Equipment Underrated? |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | With | Int |  |  |  |  |  |  |  | With | Int |
| 40MCC9201 40MCC9201 | 480 | MCCB | 2 |  | 65.0 | 1.15 | 21.6 | 21.7 | 1 | 21.6 | 1 | 3 Phase |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 40SWBD910 40SWBD9101 | 480 | MCCB | 2 |  | 50.0 | 4.54 | 33.5 | 41.0 | 1 | 33.5 | 1 | 3 Phase |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 40XFMR9201 40XFMR9201 PRI | 480 | N/A |  |  |  | 0.92 | 19.2 | 19.2 |  |  | 1 | 3 Phase |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 40XFMR920140XFMR9201 SEC | 208 | N/A |  |  |  | 0.74 | 1.1 | 1.1 |  |  | 1 | Line To Ground |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 40XFMR9202 40XFMR9202 PRI | 480 | N/A |  |  |  | 0.66 | 9.5 | 9.5 |  |  | 1 | 3 Phase |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 40XFMR920240XFMR9202 SEC | 208 | N/A |  |  |  | 0.74 | 1.0 | 1.0 |  |  | 1 | Line To Ground |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 45VFD1001 45VFD1001 | 480 | MCCB | 2 |  | 50.0 | 4.48 | 32.1 | 39.2 | 1 | 32.1 | 1 | 3 Phase |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 45VFD1003 45VFD1003 | 480 | MCCB | 2 |  | 50.0 | 4.48 | 32.1 | 39.2 | 1 | 32.1 | 1 | 3 Phase |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 45VFD1006 45VFD1006 | 480 | MCCB | 2 |  | 65.0 | 3.37 | 26.6 | 30.4 | 1 | 26.6 | 1 | 3 Phase |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 45VFD1007 45VFD1007 | 480 | MCCB | 2 |  | 65.0 | 3.21 | 25.5 | 28.8 | 1 | 25.5 | 1 | 3 Phase |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 46SWBD910 46SWBD9101 | 480 | MCCB | 2 |  | 50.0 | 3.92 | 35.8 | 42.4 | 1 | 35.8 | 1 | Line To Ground |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Low Voltage Equipment Short Circuit Summary List

| Node ID | Node Name | Volts | Type of Device | Cat | Equip Rating |  | XIR <br> Ratio | 1/2 Cycle Sym (KA) <br> (ACComp) | 1/2 Cycle Asym (KA) | MF | 1/2 Cycle <br> Sym (KA) <br> X MF | S\# | Type Of Fault | Equipment Underrated? |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | With | Int |  |  |  |  |  |  |  | With | Int |
| 46SWGR900 | 46SWGR9001 | 480 | MCCB | 2 |  | 100.0 | 4.68 | 38.3 | 47.2 | 1 | 38.3 | 1 | Line To Ground |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 50DP9201 | 50DP9201 | 480 | MCCB | 2 |  | 35.0 | 1.21 | 10.5 | 10.6 | 1 | 10.5 | 1 | 3 Phase |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 50LP9201 | 50LP9201 | 208 | MCCB | 4 |  | 10.0 | 0.75 | 2.0 | 2.0 | 1 | 2.0 | 1 | Line To Ground |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 50LP9202 | 50LP9202 | 208 | MCCB | 4 |  | 10.0 | 0.74 | 1.9 | 1.9 | 1 | 1.9 | 1 | Line To Ground |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 50XFMR9201 | 50XFMR9201 PRI | 480 | N/A |  |  |  | 1.07 | 9.8 | 9.9 |  |  | 1 | 3 Phase |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 50XFMR9201 | 50XFMR9201 SEC | 208 | N/A |  |  |  | 0.76 | 2.0 | 2.0 |  |  | 1 | Line To Ground |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 70DP9201 | 70DP9201 | 480 | MCCB | 2 |  | 35.0 | 1.15 | 7.9 | 7.9 | 1 | 7.9 | 1 | 3 Phase |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 70LP9201 | 70LP9201 | 208 | MCCB | 4 |  | 10.0 | 0.76 | 2.0 | 2.0 | 1 | 2.0 | 1 | Line To Ground |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 70LP9202 | 70LP9202 | 208 | MCCB | 4 |  | 10.0 | 0.76 | 2.0 | 2.0 | 1 | 2.0 | 1 | Line To Ground |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 70XFMR9201 70XFMR9201 PRI |  | 480 | N/A |  |  |  | 1.05 | 7.5 | 7.5 |  |  | 1 | 3 Phase |  |  |
|  |  | Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 70XFMR9201 $70 \times \mathrm{FMR9201} \mathrm{SEC}$ |  | 208 | N/A |  |  |  | 0.76 | 2.0 | 2.0 |  |  |  | Line To Ground |  |  |
|  |  | Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Low Voltage Equipment Short Circuit Summary List

| Node Name | Volts | Type of Device | Cat | Equip Rating |  | XIR <br> Ratio | 1/2 Cycle Sym (KA) (ACComp) | 1/2 Cycle Asym (KA) | MF | $\begin{gathered} \text { 1/2 Cycle } \\ \text { Sym (KA) } \\ \text { X MF } \end{gathered}$ | S\# | Type Of Fault | Equipment Underrated? |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | With | Int |  |  |  |  |  |  |  | With | Int |
| 70XFMR9202 70XFMR9202 PRI | 480 | N/A |  |  |  | 1.05 | 7.5 | 7.5 |  |  | 1 | 3 Phase |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 70XFMR9202 70 XFMR9202 SEC | 208 | N/A |  |  |  | 0.76 | 2.0 | 2.0 |  |  | 1 | Line To Ground |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| M-20MCC91 20MCC9101 MTRS | 480 | N/A |  |  |  |  |  |  |  |  |  |  |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| M-30MCC91 MTRS-30MCC9101 | 480 | N/A |  |  |  |  |  |  |  |  |  |  |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| M-40MCC92 ${ }^{\text {MTRS 40MCC9201 }}$ | 480 | N/A |  |  |  |  |  |  |  |  |  |  |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| MTR-10P100 MTR 10P1001 | 480 | N/A |  |  |  |  |  |  |  |  |  |  |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| MTR-10P100 MTR 10P1002 | 480 | N/A |  |  |  |  |  |  |  |  |  |  |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| MTR-10P100 MTR 10P1003 | 480 | N/A |  |  |  |  |  |  |  |  |  |  |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| MTR-30P100 MTR 30P1001 | 480 | N/A |  |  |  |  |  |  |  |  |  |  |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| MTR-30P100 MTR 30P1002 | 480 | N/A |  |  |  |  |  |  |  |  |  |  |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| MTR-30P760 MTR 30P7600 | 480 | N/A |  |  |  |  |  |  |  |  |  |  |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| Low Voltage Equipment Short circuit Summary List |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Node ID | Node Name | Volts | Type of Device | Cat | Equip Rating |  | XIR <br> Ratio | 1/2 Cycle Sym (KA) (ACComp) | 1/2 Cycle Asym (KA) | MF | 1/2 Cycle <br> Sym (KA) <br> X MF | S\# | Type Of Fault | Equipment Underrated? |  |
|  |  |  |  |  | With | Int |  |  |  |  |  |  |  | With | Int |
| MTR-30P860 | MTR 30P8601 | 480 | N/A |  |  |  |  |  |  |  |  |  |  |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| MTR-45P100 | MTR 45P1001 | 480 | N/A |  |  |  |  |  |  |  |  |  |  |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| MTR-45P100 | MTR 45P1003 | 480 | N/A |  |  |  |  |  |  |  |  |  |  |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| MTR-45P100 | MTR 45P1006 | 480 | N/A |  |  |  |  |  |  |  |  |  |  |  |  |
| Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| MTR-45P100 MTR 45P1007 |  | 480 | N/A |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | Comment: |  |  |  |  |  |  |  |  |  |  |  |  |  |

TAB 7

# PROTECTIVE DEVICE COORDINATION STUDY 

## Time Current Curve Discussion

The determination of a particular setting is based upon a careful balancing of the competing goals of equipment protection and pure selectivity. There are many codes that specifically define the required limits of equipment protection. Examples of these are the National Electric Code (NEC) for cable, motor, and transformer protection. The American National Standards Institute (ANSI) also has requirements for protection of transformers due to short circuits and through faults. The engineer considered these standard codes and requirements. Their applications are graphically demonstrated on the time current curves. Time current curves are logarithmic graphs of time versus current. The graphs show the devices' operational characteristic curves. The curves graphically illustrate the coordination between the devices.

The engineer made every attempt to utilize the existing equipment and determine settings to meet present day requirements and practices. The engineer must maintain a coordination margin (dependent on device type) among device characteristic curves. This ensures that only the desired unit operates and prevents more of the system from being deenergized.

The coordination study required calculating the short circuit values at the equipment and plotting these values on time current curves. The engineer plotted fuse, transformer protection, relay, and circuit breaker curves, starting from the end load and working towards the main switchgear. The study was done on the 480, and 208 -volt equipment shown on the one line drawing. The study contains time current curves, copies of the manufacturers' time current curves and tables of the low voltage circuit breaker settings.

The protective device coordination study was performed using the SKM PowerTools CAPTORS program. SKM Power Tools is a collection of programs that are used for design and analysis of power systems. The software was written and is distributed by SKM Systems Analysis Inc. of Manhattan Beach, CA.

The Time Current Curve (TCC) sheet \#1 shows the plots of the fuse, transformer and downstream 480-Volt equipment. A typical curve shows the primary device followed by other devices downstream. A TCC ID \# identifies each device on the curve. This ID number is used to locate the device in the equipment data/settings table and on the time current curve. Each time current curve contains a small one-line diagram that shows the plotted devices.

In general, most of the devices will not selectively coordinate in the instantaneous region. This is considered a tolerable situation in most cases due to the operating characteristics of these devices in that region. However, for elevator circuits, emergency systems, and

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legally required standby systems this is not acceptable per NEC code 620.62 (People Transporting Equipment), 700.27 (Emergency Systems), and 701.18 (Legally Required Standby Systems). For these areas, selective coordination is required and the protective device curves shall not overlap. In the discussions that follow, no reference will be made to this issue unless the situation merits further comment.

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## Discussion of Time Current Curves

| TCC\# | 1 | Equipment Name |
| ---: | :--- | :--- |
| Device\# | 1 | 05PMS9001 | Circuit Description

There is overlapping between the feeder breaker to 10VFD1001 (Device \#5) and 10VFD1001 breaker (Device \#6). This overlap is considered acceptable since they are in series; if either devices trip, it will have the same effect. Switchgear 15SWGR9001 Main (Device \#3) and Feeder to Switchboard 10SWBD9101 (Device \#4) over lap in the instantaneous region.

| TCC\# 1GF | Equipment Name | Circuit Description |
| ---: | :--- | :--- |
| Device\# 3 | 15SWGR9001 | MAIN |
| 4 | 15SWGR9001 | 10SWBD9101 |

The ground fault devices coordinate.

| TCC\# 2 | Equipment Name | Circuit Description |
| ---: | :--- | :--- |
| Device\# 3 | 15SWGR9001 | MAIN |
| 8 | 15 SWGR9001 | 20MCC9101 |
| 9 | $20 M C C 9101$ | LRG BRK |

The devices are coordinated in the long time and short time region.

| TCC\# 2GF | Equipment Name | Circuit Description |
| ---: | :--- | :--- |
| Device\# 3 | 15SWGR9001 | MAIN |
| 8 | 15SWGR9001 | 20MCC9101 |

The ground fault devices coordinate.

| TCC\# | 3 | Equipment Name |
| ---: | :--- | :--- |
| Device\# | 10 | 05PMS9001 |
| 11 | 05XFMR9002P |  |
| 12 | 30 SWBD9001 |  |
| 13 | 30 SWBD9001 |  |
| 14 | 30 VFD1001 |  |

Circuit Description<br>05XFMR9002 PRI<br>Transformer Damage Curve MAIN<br>30VFD1001<br>VFD BREAKER

Tab 7 Page 3

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15 MTR-30P1001
Motor Starting Curve
There is overlapping between the feeder breaker to 30VFD1001 (Device \#13) and 30VFD1001 breaker (Device \#14). This overlap is considered acceptable since they are in series; if either devices trip, it will have the same effect. There is also some overlap of all devices in the instantaneous region.

| TCC\# 4 | Equipment Name | Circuit Description |
| ---: | :--- | :--- |
| Device\# 16 | 05PMS9002 | 05XFMR9004 PRI |
| 17 | 05XFMR9004P | Transformer Damage Curve |
| 18 | 46SWGR9001 | MAIN |
| 19 | 46SWGR9001 | 46SWBD9101 |
| 20 | 46SWBD9101 | 45VFD1001 |
| 21 | 45VFD1001 | VFD BREAKER |
| 22 | MTR-45P1001 | Motor Starting Curve |

There is overlapping between the feeder breaker to 45VFD1001 (Device \#20) and 45VFD1001 breaker (Device \#21). This overlap is considered acceptable since they are in series; if either devices trip, it will have the same effect. There is also some overlap of all devices in the instantaneous region.

| TCC\# 4GF | Equipment Name |  |
| ---: | :--- | :--- |
| Device\# | 18 | 46SWGR9001 |
|  | 19 | 46SWGR9001 |

Circuit Description
MAIN
46SWBD9101
The ground fault devices coordinate.

| TCC\# 5 | Equipment Name | Circuit Description |
| ---: | :--- | :--- |
| Device\# 19 | 46SWGR9001 | 46SWBD9101 |
| 23 | 46SWBD9101 | 45VFD1006 |
| 24 | 45VFD1006 | VFD BREAKER |
| 25 | MTR-45P1006 | Motor Starting Curve |

There is overlapping between the feeder breaker to 45VFD1006 (Device \#23) and 45VFD1006 breaker (Device \#24). This overlap is considered acceptable since they are in series; if either devices trip, it will have the same effect. There is also some overlap of all devices in the instantaneous region.

| TCC\# | 6 | Equipment Name | Circuit Description |
| ---: | :--- | :--- | :--- |
| Device\# | 18 | $46 S W G R 9001$ | MAIN |
| 26 | $46 S W G R 9001$ | $40 S W B D 9101$ |  |
| 27 | $40 S W B D 9101$ | $40 M C C 9201$ |  |

The devices are coordinated in the long time and short time region. There is also some

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overlap of all devices in the instantaneous region.

TCC\# 6GF Equipment Name
Device\# 18 46SWGR9001
26 46SWGR9001

## Circuit Description

MAIN
40SWBD9101

The ground fault devices coordinate.

TAB 8


TCC Sheet: 1-Fdr to 05XFMR9001, 05XFMR9001 Crv, 15SWGR9001 Mn, Fdr to 10SWBD9101, Fdr to 10VFD1001, 10VFD1001 Brk, and 10 P 1001 I

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$\stackrel{\text { 丷ㅡㄹ }}{ }^{0}$
TCC Sheet: 1GF-15SWGR9001 Main and Feeder to 10SWBD9101

Oneline: tcc1
April 28, 2011 10:20 AM
SKM Systems Analysis, Inc.

Fault Type: InitSym SLG
1
10
은
$\underset{\sim}{V}$
음
3-15SWGR9001 MN
SIEMENS
WL, ETU745, Size II II
WLL, Size II
Trip 3200.0 A
Plug 1600.0 A
Plug 1600.0 A
Settings Phase
Settings Phase
LTPU, $(0.4-1 \times$ P) 1 (1600A)
LTD-I2t, (2-30s) 5.5
STPU, ( $1.25-12 \times$ P) 2 ( 3200 A )
STD, ( $0.1-0.4 \times$ P) 0.2 (I^2t Out)
INST, ( $1.5-12 \times$ P), AETU 12 (19200


TCC Sheet: 2-15SWGR9001 Main, Feeder to 20MCC9101, and 20MCC9101 Largest Breaker

## CURRENT IN AMPERES



## CURRENT IN AMPERES



TCC Sheet: 3-Fdr to 05XFMR9002, 05XFMR9002 Crv, 30SWBD9001 Mn, Fdr to 00VFD1001, 30VFD1001 Brk, and 30P1001 Mtr Crv

Fault Type: InitSym 3P

## CURRENT IN AMPERES



TCC Sheet: 4-Fdr to 05XFMR9004, 05XFMR9004 Crv, 46SWGR9001 Mn, Fdr to 46SWBD9101, Fdr to 45VFD1001, 45VFD1001 Brk, and 45P1001 I

## CURRENT IN AMPERES




TCC Sheet: 5-Feeder to 46SWBD9101, Feeder to 45VFD1006, 45VFD1006 Breaker, and 45P1006 Motor Curve

Current Scale x 100
Reference Voltage: 480
Fault Type: InitSym 3P

## CURRENT IN AMPERES



TCC Sheet: 6-46SWGR9001 Main, Feeder to 40SWBD9101, and Feeder to 40MCC9201

Fault Type: InitSym 3P

18-46SWGR9001 MN SIEMENS WL, ETU745, Size III WLL, Size III Trip 4000.0 A Plug 2500.0 A
Settings Ground Ig, ( $400-1200 \mathrm{~A}) \mathrm{E}(1200 \mathrm{~A})$ $\operatorname{tg},(0.1-0.5 \mathrm{~s}) 2(1 \wedge 2 \mathrm{t} \mathrm{ln})$
26-FDR TO 40SWBD9101 SIEMENS
WL, ETU745, Size I
WLL, Size I
Trip 800.0 A
Plug 600.0 A
Settings Ground
Ig, ( $100-1200 \mathrm{~A}) \mathrm{B}(300 \mathrm{~A})$
tg, ( $0.1-0.5 \mathrm{~s}) 0.1$ (॥^2t In)

TCC Sheet: 6GF-46SWGR9001 Main and Feeder to 40SWBD9101

Fault Type: InitSym SLG

TAB 9

## Solid State \& Thermal/Magnetic Molded Case Circuit Breaker Settings (with Instantaneous Settings only)

\(\left.\begin{array}{|ll|}\hline - Feeder Breakers Feeding Panelboards* \& Set instantaneous to Maximum <br>
- Feeder Breakers Feeding Dry type \& Set instantaneous to Maximum <br>

transformers*\end{array}\right]\)| - Panelboard Main Breakers* - | Set instantaneous to Maximum |
| :--- | :--- |
| Branch Breakers * |  |


| - Breaker Pick Up or Overload Settings for Motor Circuits* |  |
| :---: | :---: |
| Motor Service Factor - $\mathbf{1 . 1 5}$ | Setting <125\% x I(nameplate Amps) <br> (Up to $140 \%$ if nuisance tripping occurs) |
| Motor with Temp Rise $40^{\circ} \mathrm{C}$ | Setting $<125 \% \times$ I(nameplate Amps) <br> (Up to $140 \%$ if nuisance tripping occurs) |
| All other Motors | Setting $<115 \% \times$ I(nameplate Amps) <br> (Up to $130 \%$ if nuisance tripping occurs) |


| •Breaker Overcurrent for Motor Circuits* |  |
| :--- | :--- |
| Inverse Time Breaker | Setting <250\% x I(nameplate Amps) |
| Instantaneous Trip Breaker | Setting <800\% x I(nameplate Amps) <br> (For non Design E or B Energy <br> Efficiency Motors) |
|  | Setting <1,100\% x I(nameplate Amps) <br> (For Design E or B Energy Efficiency <br> Motors) |
|  | Setting <1,300\% x I(nameplate Amps) <br> (For non Design E or B Energy |
| Combination Controller - <br> Instantaneous Trip Breaker <br> (NEC Table 430.52 Exception if motor <br> trips using the values above.) | Efficiency) |
|  | Setting <1,700\% x I(nameplate Amps) <br> (For Design E or B Energy Efficiency |
|  | Motors) |

[^0]TAB 10

## SMU FUSE UNITS—S\&C SLOW SPEED

BASIS-These fuse units are tested in accordance with the procedures described in ANSI Standard C37.41-1981, and they are rated to comply with ANSI Standard C37.46-1981. As required by these
standards, the minimum melting current is not less than $200 \%$ of standards, the minimum melting current is not less than $200 \%$ of on tests starting with the fuse unit at an ambient temperature of $25^{\circ} \mathrm{C}$ and no initial load.

CONSTRUCTION-Fusible elements are silver, helically coiled, and of solderless construction.
TOLERANCES-Curves are plotted to minimum test points. Max imum variations expressed in current values are plus $10 \%$.
APPLICATION-Like all high-voltage fuses, these fuse units are intended to accommodate overloads, not to interrupt them. Accordingly, they feature fusible elements which are designed with a minimum melting current of $200 \%$ of the fuse-unit ampere rating (for fuse units rated 100 amperes or less) or $240 \%$ of the fuse-unit ampere rating (for fuse units rated over 100 amperes). As a result, these fuse units have considerable peak-load capabilities; however,
they should never be exposed to loading in excess of the peak-load they should never be exposed to loading in exce
capabilities listed in S\&C Data Bulletin 240-190.

Since these fuse units have silver element construction which is en to damage by aging or transient overcurrents it is unne essary to replace unblown fuse units in single-phase or three-phase installations when one or more fuse units have blown.

COORDINATION-Any preloading reduces melting time. While this phenomenon is especially pronounced in other makes of fuses rating, the effect of preloading must nonetheless be determined for the S\&C fuse units represented by these curves (see S\&C Data Bulletin 240-195) and adjustments to these curves must be made: 1. When close coordination is required;
2. When, regardless of the preciseness of coordination, the fuse ed to temporary overloads.
There are cases where the coordination requirements may be very exacting, for example, in coordinating a transformer primary use with a secondary breaker and a source-side breaker. The time interval between the operating characteristics of the two breakers may be very narrow. Under these circumstances there must be an xitremely short time interval between the minimum melting and the otal clearing characteristics of the fuse
The fuse units represented by these curves possess this short
me interval feature, since--having a nondamageable fusible element of precise construction-they require
. As little as $10 \%$ total tolerance in melting current-compared to
the $20 \%$ tolerance of many fuses ( $20 \%$ and $40 \%$ respectively in terms of time).
This narrow time band normally will provide the desired coordination. If the selected S\&C Slow Speed fuse unit does not meet the in the S\&C Very Slow Speed will satisfy.

Sometimes a selected ampere rating will fail to meet the coordi nation requirements in any available speed. In this case the selec-
tion of another ampere rating for either the proctecting tion of another ampere rating for eithe
fuse usually will satisfy all requirements.
Do nily watisfy all re
Do not assume that other fuses that do not employ S\&C's silver
helically coiled fusible
 coordination impasse than the use of another ampere rating in one of the S\&C speed options. Such other fuses, including "time-lag speeds, "super-slow" speeds, and "high-surge" speeds, require the use of "safety-zone" or setback allowances and, in addition, they have larger construction tolerances (plus 20\% in current; plus $40 \%$ in terms of time). The application of these two factors wili give a time clearing curve greater than in the case of $\mathrm{S} \& \mathrm{C}$ speed options.

## FUSE UNITS AVAILABLE- <br> Type <br> Iype Kv Nom. Ratings SMD-40@ .......... 14.4 through 34.5

Ampere Ratings AE through 200
$\star$ These curves are also applicable to a previous design desig nated SMD-20.


MINIMUM MELTING TIME-CURRENT CHARACTERISTIC CURVES
 lo tomply with ANS Standant C37 48-1981. As redurach ky tese standiaria. Ma ninithion matiting current is rol less then $200 \%$ baedd ontests stanting wint ine reflif unit tatsn ambient tampergurs of $25^{\circ} \mathrm{C}$ and no notsil oad
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 adyition, thes have large constiction to termes fatus zais in cures plus sät in terme of time: The apsileation of trese iw taciors wil give a lime interval betwoen the adjusied minimuin mest ry su:w enkl the totat elpuing gume greater than in the a ace c! ste zaped options





# ARC FLASH STUDY 

## Arc Flash Calculations

The protection engineer performed arc flash calculations to determine the incident energy and arc flash boundary for various locations throughout the power system. Once the incident energy and arc flash boundaries are known, the required PPE is determined and the appropriate arc flash warning labels are generated. The owner can then attach these warning labels to electrical equipment that would require servicing while energized. These labels will indicate to personnel what the arc flash boundary is and what the correct personal protective equipment (PPE) is that they are required to wear.

## CAUTION!

The equations used for the calculation of the estimated maximum incident energy and the estimated arc flash boundary distance are still under review and testing by IEEE and others.

Users should be aware that the equations are based upon measured incident energy under a specific set of test conditions and on theoretical work. Actual arc flash exposures may be more or less severe than calculated by the PTW program. (A discussion of the PTW program used for our calculations follows.) Calculations are base on the installation and configuration of the electrical distribution system as initially constructed. Any changes or additions of the electrical distribution system may cause these calculations to be null \& void. All short circuit and overcurrent protective devices (OCPD) must be replaced with the exact same manufacturer and model. Also, the user should beware of the potentially hazardous effects of molten copper splatter, pressure impulses (arc blast), toxic arc byproducts, and projectiles. These effects have not been considered in the equation.

Personal Protective Equipment (PPE) for the arc flash hazard is the last line-of-defense. It is not intended nor will it prevent all injuries. NFPA 70E (2009) PPE levels are intended to reduce the impact of an arc flash to $2^{\text {nd }}$ degree burns for the torso and head only. NFPA 70E (2009) states that the incident energy exposure shall be based on the working distance of the employee's face and head (18"). Objects closer to the arc flash will be exposed to much greater levels of incident energy. Fire Rated (FR) clothing and PPE shall be used based upon the incident energy exposure. This means injuries to hands and arms are expected if an arc at the level calculated and protected against occurs. It is impossible to design PPE to prevent all injures since it would be very restrictive and difficult to work in.

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#### Abstract

Incident energy levels are directly related to the clearing time of the upstream OCPD. Operation of the OCPD within the manufacturers design specifications is essential for limiting the incident energy due to arc flash hazards. The Arc Flash Hazard Study is calculated based on the manufacturers published time current curves for new equipment. Failure of the OCPD components to operate within the manufacturer's time current curves will compromise the results of this Arc Flash Study and will result in higher levels of incident energy to electrical workers. NFPA 70E (2009) \& 70B standards recommend regularly scheduled maintenance and testing be performed on the electrical distribution system components to assure proper operation of all over current protective devices. Regular testing is required to protect electrical workers from greater arc flash energy hazards than are calculated in this study.


The engineer performed the arc flash calculations for the equipment shown on the electrical one line drawing contained in the report. The engineer started at the utility main service and continued downstream to include the equipment shown of the one line drawings.

## PTW Arc Flash Evaluation Program

The protection engineer used the PTW (Power Tools for Windows) Arc Flash Evaluation program. SKM System Analysis, Inc. of Manhattan Beach, CA, wrote this program. It is an accepted industry standard for arc flash calculations. This program calculates the incident energy and arc flash boundary based upon the three-phase short circuit duties at each bus and through each protective device.

The arcing fault current through the protective devices is then calculated from the bolted fault value and used to automatically find the time duration of the arc from the time current coordination (TCC) curves. Incident energy and arc flash boundaries are calculated based on the bus three-phase fault current and arcing duration. Clothing requirements are specified from a user defined personal protective equipment table.

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The PTW Arc Flash program created the table above. Reading from left to right, the columns have the following definitions:

| Bus Name: | Indicates the fault location. |
| :---: | :---: |
| Protective Device Name: | The first protective device in each parallel branch feeding the fault. |
| kV: | Bus voltage at the fault location. |
| Bus Bolted Fault: | Total symmetrical fault current at the fault location. |
| Prot Dev Bolted Fault: | Symmetrical fault current passing through the referenced protective device for a bolted fault at the fault location, referenced to bus voltage at fault location. |
| Arcing Fault: | Branch fault current passing through the referenced protective device for an arcing fault at the fault location, referenced to bus voltage at fault location. |
| Trip/Delay Time: | Time for referenced protective device to trip (clearing curve) at arcing fault branch current value. |
| Breaker Opening Time: | User-defined trip time for breaker used when protective device clearing curve does not include the breaker operating time. For example, published relay trip curves reflect only the trip time of the relay since they can be applied to many different breakers and therefore the breaker opening time needs to be included. |
| Ground: | 'Yes' indicates that the fault bus is connected solidly to ground. 'No' indicates that the fault bus is resistance grounded or ungrounded. The empirical equations for incident energy vary for grounded and ungrounded systems. |
| In Box: | Identifies whether the fault location is in an enclosure or in open air. In open air the arc energy will radiate in all directions whereas an enclosure will focus the energy toward the enclosure opening. The In Box / Air selection is available when the NFPA 70E (2009) study option is selected. For the IEEE 1584 (2002) study selection the In Box or In Air is determined automatically from the Equipment Type specification. |
| Equip Type: | Used only in the IEEE 1584 (2002) method to determine In Box or In Air condition as well as to provide a default gap between bus bars and distance factor used in the incident energy calculation. |
| Gap: | Gap between conductors where arc will occur. |

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| Arc Flash Boundary: | Minimum distance from the arc within which a second degree <br> burn could occur if no protective clothing is worn. |
| :--- | :--- |
| Working Distance: | Closest distance a worker's body, excluding arms and hands, <br> would be exposed to the arc. |
| Incident Energy: | Energy released at the specified working distance expressed in <br> cal/cm2 or J/cm2. |
| Clothing Class: | Minimum clothing class designed to protect worker from second- <br> degree burns. |

The following assumptions have been made by the PTW programmers and PowerStudies.com Protection Engineer:

1. Arc Flash searches up to 5 branches away from the faulted bus to find the fastest protective device with an over-current trip curve. The device with the fastest trip time for the given arcing fault current is used. In most situations, this is the device closes to the faulted bus.
2. Worker is stationary during the entire arc flash incident (constant working distance) up to 2.0 seconds.
3. The maximum time that a worker will be exposed to the arc flash is 2.0 seconds. Either the person will move away or be blown away from the arcing fault location.
4. Induction motors are assumed to be operating. Fault current contribution from the motors lasts for 6 cycles only.
5. Current-limiting range for fuses is assumed to start where fuse clearing curve crosses 0.01 sec .
6. Current-limiting fuses operating in current limiting range are assumed to clear in $1 / 2$ $1 / 4$ cycle.
7. The Interrupting device is rated for available short circuit current.
8. Upstream branch devices are properly coordinated with downstream branch devices and are set to the values specified in the protective device coordination study performed by PowerStudies.com.
9. The engineer performed the arc flash calculations for the equipment shown on the electrical one line drawing contained in the report. The engineer started the utility main service and continued downstream.

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## Theory

Arc Flash Evaluation is calculated using IEEE 1584 (2004a) Standard. The Arc Flash Evaluation Program uses the following calculation procedures to determine the values shown on the Arc Flash Warning Labels and in the Arc Flash Evaluation Bus Reports.:

## Arc Flash Evaluation Using IEEE 1584 (2004a)

The following equations are reprinted with permission from IEEE 1584 (2004a) *Copyright 2004*, by IEEE. The IEEE disclaims any responsibility or liability resulting from the placement and use in the described manner.

1) Arc Flash Evaluation using IEEE 1584 (2002a) / D10 assumes that the following ranges are used.
a) Range of the model
b) Bus Voltage between 208 V and 15 kV
c) Bolted fault current at the bus between 700 A and 106 kA
d) Bus bar gap between 13 mm and 153 mm
e) For systems outside these ranges, use the LEE equation instead
2) Determine the 3 Phase Fault at each bus in the power system, calculate or determine the Bolted Fault Current at the bus (IB) and the Bolted Fault Current through each protective device (IB br).
3) Determine the Arcing Fault Current at the bus (la) and through each protective device (la br).

For low voltage distribution systems, nominal voltage $<1 \mathrm{kV}$ and $700 \mathrm{~A} \leq \mathrm{IB} \leq 106 \mathrm{kA}$
$\lg (\mathrm{la})=\mathrm{K}+0.662 \lg (\mathrm{IB})+0.0966 \mathrm{~V}+0.000526 \mathrm{G}+0.5588 \mathrm{~V} \lg (\mathrm{IB})-0.00304 \mathrm{G} \lg$ (IB)

Ig is $\log 10$
la is arcing fault current at the bus
$\mathrm{K} \quad$ is -0.153 for open configuration and
is -0.097 for box configuration
IB is bolted fault current - 3phase sym rms kA at the bus
V is bus voltage in kV
G is bus bar gap between conductors in mm
For medium voltage bus systems with nominal voltage $\geq 1 \mathrm{kV}$ and $700 \mathrm{~A} \leq \mathrm{IB} \leq 106 \mathrm{kA}$
$\lg (\mathrm{la})=0.00402+0.983 \lg (\mathrm{IB})$
Therefore, $\quad l a=10 \lg (\mathrm{la})$
la $\mathrm{br}=\mathrm{la}$ * IB br / IB
IB br $\quad$ is the Bolted Fault Current through each protective device. la br is the arcing fault current through each protective device.
*Note: Following IEEE 1584 (2002) - 5.2, we are calculating a second arcing fault current at $85 \%$ of the original, calculate the Trip Time and Incident Energy at both 85\% and $100 \%$ arcing fault current and display the larger of the two Incident Energy values with the associated Trip Time.
4) Determine the Trip/Delay time for fuses from the Time Current Coordination Curve (TCC).

Standard fuses that have both minimum melting and total clearing curves available, use the trip time read from the total clearing time curve. For fuses with only the average melting time curve available, the time Tr used is from the average melting curve at the arcing current level. If Tr is less than or equal to 0.03 seconds, then $15 \%$ additional delay is added to Tr . If Tr is above 0.03 seconds, then $10 \%$ is added to Tr and this value is used for the total clearing time.

For standard fuses, if the arcing fault current is above the total clearing time at the bottom of the curve (0.01s), then 0.01s is used to Tr. (IEEE_P1584/D10 Pg 7)

For all current limiting fuses and breakers, if the trip time read from the TCC clearing curve at the branch arcing fault current is less than $1 / 2$ cycles, then this value is used as the trip time. Otherwise, define the current at 0.01 seconds as the IL, and la as the arcing fault current at the protective device:

Trip/Delay Time
Read from clearing curve
1/2 cycles*
$\mathrm{IL} \leq \mathrm{la} \leq 2 \mathrm{IL}$
1/4 cycles**
la>2IL

*     - The Current limiting devices are not assumed to be current limiting for this lower value of la.
** - The current limiting devices are assumed to be current limiting for this higher value of la.

5) Determine the Trip/Delay time for relays from the TCC.

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Use the TCC curve and read the Read Trip/Delay time. Use 16 ms for relays that operate instantaneously and add the circuit breaker opening time.

Breaker Opening Time For relays:
Breaker Opening Time Breaker Rating and Type
1.5 cycle
3.0 cycle
5.0 cycle
8.0 cycle
< 1000 V molded case
< 1000 V power circuit
$1-35 \mathrm{kV}$
$>35 \mathrm{kV}$
For low voltage circuit breakers that can be tripped by relays, use a breaker opening time of 3 cycles. For all other device categories, set the Breaker Opening Time to 0.0s since the Trip/Delay Time reading from the TCC include breaker opening time already
6) Determine the Arcing duration by adding the Trip/Delay time and Breaker Opening time.
7) Determine the Equipment Type and Bus Bar Gap.

IEEE1584 lists four Equipment Types. They are Switchgear, Panel, Cable, and Open Air. The following defaults are used according to the voltage level.

| Equipment Type | kV |
| :--- | :--- |
| Panel | $\leq 1$ |
| Switchgear | $\leq 35$ |
| Air | $>35$ |
| Panel | $\leq 1$ |


| Classes of Equipment | Gap (mm) |
| :--- | :--- |
| $\leq 1 \mathrm{kV}$ Switchgear | 32 |
| $\leq 1 \mathrm{kV}$ MCCs and Panelboards | 25 |
| $1-5 \mathrm{kV}$ Switchgear | 104 |
| $>5 \mathrm{kV}$ Switchgear | 153 |
| All Cable | 13 |
| $1-5 \mathrm{kV}$ Open Air | 104 |
| $>5 \mathrm{kV}$ Open Air | 153 |

8) Determine the Working Distance

The working distance based on the voltage level and equipment type using the table below.

| Working Distance | Equipment Type | kV |
| :--- | :--- | :--- |
| 24 inches $(610 \mathrm{~mm})$ | Switchgear | $\leq 1$ |

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| 18 inches $(455 \mathrm{~mm})$ | Panel | $\leq 1$ |
| :--- | :--- | :--- |
| 36 inches $(910 \mathrm{~mm})$ | Switchgear | $>1 \&<35$ |
| 72 inches $(1829 \mathrm{~mm})$ | Switchgear | $>35$ |
| 18 inches $(455 \mathrm{~mm})$ | all others |  |

9) Determine whether the equipment is grounded or not
10) Calculate the Incident Energy
$\lg (E n)=K 1+K 2+1.081 \lg (\mathrm{la})+0.0011 G$
En is incident energy ( $\mathrm{J} / \mathrm{cm} 2$ ) normalized for an arcing duration of 0.2 s and working distance of 610mm
$\mathrm{K} 1 \quad$ is -0.792 for open configuration and is -0.555 for box configuration (switchgear, panel, cable)
K2 is 0 for ungrounded and high resistance grounded systems and is -0.113 for grounded systems
G is the gap between bus bar conductors in mm
solve $E n=10 \mathrm{lg}$ En
Incident Energy is converted from normalized:
$E=4.184 \mathrm{Cf}$ En (t/0.2) (610X / DX)
Eis incident energy ( $\mathrm{J} / \mathrm{cm} 2$ )
$\mathrm{Cf} \quad$ is 1.0 for voltage above 1 kV and
is 1.5 for voltage at or below 1 kV
$t$ is arcing duration in seconds
D is the working distance
$x$ is the distance exponent
The distance exponent $x$ based on the voltage level and equipment type shown in the table below.
x
1.473
1.641
0.973

2

| Equipment Type | kV |
| :--- | :--- |
| Switchgear | $\leq 1$ |
| Panel | $\leq 1$ |
| Switchgear | $>1$ |
| all others |  |

11) Calculate the Arc Flash Boundary DB

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$D B=\left[4.184 \mathrm{Cf} \mathrm{En}(\mathrm{t} / 0.2)\left(610^{\wedge} \mathrm{X} / \mathrm{EB}\right)\right]^{\wedge} 1 / \mathrm{X}$

DB is the arc flash boundary in mm at incident energy of EB
$E B \quad$ is the limit for a second-degree bare skin burn. $E B=5.0(\mathrm{~J} / \mathrm{cm} 2)$
For all current limiting fuses and breakers with the manufacturer's incident energy and flash boundary equations available, the manufacturer's current limiting equations are used instead of the above equations. The current limiting equations can be entered and are stored in the protective device library.

IE = A * lbf + B - Incident Energy
$\mathrm{Db}=\mathrm{D} * \mathrm{lbf}+\mathrm{D} \quad$ - Flash Boundary
Constants $A, B, C$ and $D$ are different for different manufacturers, frames/cartridges and current ratings. If the equation is available for Incident Energy, but NOT for Flash Boundary Db, calculate IE from the current limiting equation and Db using the standard IEEE1584 equation.

If a bus has multiple contributions, calculate the incident energy from each current limiting device using the current limiting equations. Subtract these contributions from current limiting devices out of the total bolted bus fault current. Use the remaining arcing fault current and the standard IEEE1584 incident energy equations to calculate the incident energy. Add the incident energy from current limiting and none-current limiting devices together. Always calculate the Flash Boundary using the standard IEEE1584 equation when multiple contributions exist at the bus.
*Note: Following IEEE 1584 (2002) - 5.2, The program calculates a second arcing fault current at $85 \%$ of the original. Then the Trip Time and Incident Energy at both $85 \%$ and $100 \%$ arcing fault current is compared and the larger of the two Incident Energy values with the associated Trip Time are displayed.
12) Determine the PPE Clothing Class

The PPE clothing class is determined based upon the incident energy and voltage class. This table (NPFA 70E Table 130.7.C) is shown on the next few pages.

## Combined Personnel Protective Equipment Matrix Table

(Data From 2009 Edition of NFPA 70E Tables 130.7 (C)(10) and 130.7(C)(11))

| Hazard/Risk Category | Protective Clothing and PPE | PPE Clothing <br> Characteristics and Descriptions | Required Minimum Arc Rating of PPE [J/cm2(cal/cm2)] |
| :---: | :---: | :---: | :---: |
| Hazard/Risk Category 0 Protective Clothing, Non-melting (according to ASTM F 1506-00) or Untreated Natural Fiber <br> FR Protective Equipment | Shirt (long sleeve) <br> Pants (long) <br> Safety glasses or safety goggles (SR) Hearing protection (ear canal inserts) Leather gloves (AN) (Note 2) | Non-melting, flammable material (i.e., untreated cotton, wool, rayon, or silk, or blends of these materials) with a fabric weight at least $4.5 \mathrm{oz} / \mathrm{yd}^{2}$ | N/A |
| Hazard/Risk Category 1 <br> FR Clothing, Minimum Arc Rating of 4 (Note 1) <br> FR Protective Equipment | Arc-rated long-sleeve shirt (Note 3) <br> Arc-rated pants (Note 3) <br> Arc-rated coverall (Note 4) <br> Arc-rated face shield or arc flash suit hood (Note 7) <br> Arc-rated jacket, parka, or rainwear (AN) <br> Hard hat <br> Safety glasses or safety goggles (SR) <br> Hearing protection (ear canal inserts) <br> Leather gloves (Note 2) <br> Leather work shoes (AN) | Arc-rated FR shirt and FR pants or FR coverall | 16.74 (4) |
| Hazard/Risk Category 2 <br> FR Clothing, Minimum Arc Rating of 8 (Note 1) <br> FR Protective Equipment | Arc-rated long-sleeve shirt (Note 5) <br> Arc-rated pants (Note 5) <br> Arc-rated coverall (Note 6) <br> Arc-rated face shield or arc flash suit hood (Note 7) <br> Arc-rated jacket, parka, or rainwear (AN) <br> Hard hat <br> Safety glasses or safety goggles (SR) <br> Hearing protection (ear canal inserts) <br> Leather gloves (Note 2) <br> Leather work shoes | Arc-rated FR shirt and FR pants or FR coverall | 33.47 (8) |

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| Hazard/Risk Category | Protective Clothing and PPE | PPE Clothing <br> Characteristics and Descriptions | Required Minimum Arc Rating of PPE [J/cm2(cal/cm2)] |
| :---: | :---: | :---: | :---: |
| Hazard/Risk Category 3 <br> FR Clothing, Minimum Arc Rating of 25 (Note 1) <br> FR Protective Equipment | Arc-rated long-sleeve shirt (AR) (Note 8) <br> Arc-rated pants (AR) (Note 8) <br> Arc-rated coverall (AR) (Note 8) <br> Arc-rated arc flash suit jacket \& pants (AR) (Note 8) <br> Arc-rated arc flash suit hood (Note 8) <br> Arc-rated jacket, parka, or rainwear (AN) <br> Hard hat <br> FR hard hat liner (AR) <br> Safety glasses or safety goggles (SR) <br> Hearing protection (ear canal inserts) <br> Arc-rated gloves (Note 2) <br> Leather work shoes | Arc-rated FR shirt and FR pants or FR coverall, and arc flash suit selected so that the system arc rating meets the required minimum | 104.6 (25) |
| Hazard/Risk Category 4 <br> FR Clothing, Minimum Arc Rating of 40 (Note 1) <br> FR Protective Equipment | Arc-rated long-sleeve shirt (AR) (Note 9) <br> Arc-rated pants (AR) (Note 9) <br> Arc-rated coverall (AR) (Note 9) <br> Arc-rated arc flash suit jacket \& pants (AR) (Note 9) <br> Arc-rated arc flash suit hood (Note 9) <br> Arc-rated jacket, parka, or rainwear (AN) <br> Hard hat <br> FR hard hat liner (AR) <br> Safety glasses or safety goggles (SR) <br> Hearing protection (ear canal inserts) <br> Arc-rated gloves (Note 2) <br> Leather work shoes | Arc-rated FR shirt and FR pants or FR coverall, and arc flash suit selected so that the system arc rating meets the required minimum | 167.36 (40) |

## NFPA 70E Table 130.7(C)(10) Notes

## Legend:

AN = As needed (optional)
$A R=A s$ required
$S R=$ Selection required
Notes:

1. Information taken from Table $130.7(\mathrm{C})(11)$ and is shown in the last two columns. Arc rating for a garment or system of garments is expressed in $\mathrm{cal} / \mathrm{cm}^{2}$.
2. If rubber insulating gloves with leather protectors are required by Table $130.7(\mathrm{C})(9)$, additional leather or arc-rated gloves are not required. The combination of rubber insulating gloves with leather protectors satisfies the arc-flash protection requirement.
3. The FR shirt and pants used for Hazard/Risk Category 1 shall have a minimum arc rating of 4 .
4. Alternate is to use FR coveralls (minimum arc flash rating of 4) instead of FR shirt and FR pants.
5. FR shirt and pants used for Hazard/Risk Category 2 shall have a minimum arc rating of 8 .
6. Alternate is to use FR coveralls (minimum arc flash rating of 8 ) instead of FR shirt and FR pants.
7. A face shield with a minimum arc rating of 4 Hazard/Risk Category 1 or minimum are rating of 8 for Hazard/Risk Category 2, with wrap-around guarding to protect not only the face, but also the forehead, ears, and neck (or, alternatively, an arc-rated arc-flash suit hood), is required.
8. An alternate is to use a total Fr clothing system and hood, which shall have a minimum arc rating of 25 for Hazard/Risk 3.
9. The total clothing system consisting of FR short and pants and/or FR coveralls and/or arc-flash coat and pants and hood shall have a minimum arc rating of 40 for Hazard/Risk Category 4.
10. Alternate is to use a face shield with a minimum arc rating of 8 and a balaclava (sock hood) with a minimum arc rating of 8 and which covers the face, head and neck except for the eye and nose areas.
13) The Glove Rating class is determined based upon the voltage class.
14) Determine the Limited Approach Boundary

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This is the distance from an exposed live part within which a shock hazard exists. This value is determined by NFPA 70E (2009) Table 130.2(C).
15) Determine the Prohibited Approach Boundary

This is the distance from an exposed live part within which work is considered the same as making contact with the live part. This value is determined by NFPA 70E (2009) Table 130.2(C).
16) Determine the Restricted Approach Boundary

This is the distance from an exposed live part within which there is an increased risk of shock, due to electrical arc over combined with inadvertent movement, for personnel working in close proximity to the live part. This value is determined by NFPA 70E (2009) Table 130.2(C) shown below.

| (1) | (2) <br> Limited Approach <br> Boundary - Exposed <br> Movable Conductor |  | (3) <br> Limited Approach <br> Boundary - Exposed <br> Fixed Circuit Part |  | (4) Restricted Approach Boundary - Includes Inadvertent Movement Adder |  | (5) <br> Prohibited Approach Boundary |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Nominal System Voltage Range, Phase to Phase |  |  |  |  |  |  |  |  |
| Less than 50 | Not Specified |  | Not Specified |  | Not Specified |  | Not Specified |  |
| 50 to 300 | 10 ft 0 in . | 3.05 m | 3 ft in | 1.07 m | Avoid Co |  | Avoid Con |  |
| 301 to 750 | 10 ft 0 in . | 3.05m | 3 ft 6 in . | 1.07m | 1 ft 0 in . | $\begin{aligned} & 304.8 \\ & \mathrm{~mm} \end{aligned}$ | 0 ft 1 in . | $\begin{aligned} & 25.4 \\ & \mathrm{~mm} \end{aligned}$ |
| 751 to 15 kV | 10 ft 0 in. | 3.05 m | 5 ft 0 in . | 1.53 m | 2 ft 2 in . | $\begin{aligned} & \hline 660.4 \\ & \mathrm{~mm} \end{aligned}$ | 0 ft 7 in . | $\begin{aligned} & 177.8 \\ & \mathrm{~mm} \end{aligned}$ |
| 15.1 kV to 36 kV | 10 ft 0 in . | 3.05 m | 6 ft 0 in . | 1.83 m | 2 ft 7 in . | $\begin{aligned} & 787.4 \\ & \mathrm{~mm} \end{aligned}$ | 0 ft 10 in . | 254 mm |
| 36.1 kV to 46 kV | 10 ft 0 in . | 3.05 m | 8 ft 0 in . | 2.44 m | 2 ft 9 in . | $\begin{aligned} & 838.2 \\ & \mathrm{~mm} \end{aligned}$ | 1 ft 5 in . | $\begin{aligned} & 431.8 \\ & \mathrm{~mm} \end{aligned}$ |
| $\begin{aligned} & 46.1 \mathrm{kV} \text { to } 72.5 \\ & \mathrm{kV} \end{aligned}$ | 10 ft 0 in . | 3.05 m | 8 ft 0 in | 2.44 m | 3 ft 3 in . | 1 m | 2 ft 2 in . | 660 mm |
| $\begin{aligned} & 72.6 \mathrm{kV} \text { to } 121 \\ & \mathrm{kV} \end{aligned}$ | 10 ft 8 in . | 3.25 m | 8 ft 0 in . | 2.44 m | 3 ft 4 in . | 1.29 m | 2 ft 9 in . | 838 mm |
| $\begin{aligned} & 138 \mathrm{kV} \text { to } 145 \\ & \mathrm{kV} \end{aligned}$ | 11 ft 0 in. | 3.36 m | 10 ft 0 in . | 3.05 m | 3 ft 10 in . | 1.15 m | 3 ft 4 in . | 102 mm |

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| (1) | (2) |  | (3) |  | (4) |  | (5) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Nominal System | Limited Approach |  | Limited Approach |  | Restricted Approac |  | Prohibited Approach |  |
| Voltage Range, Phase to Phase | Boundary - Exposed |  | Boundary - Exposed |  | Boundary - Includes |  | Boundary |  |
|  | Movable Conductor |  | Fixed Circuit Part |  | Adder |  |  | 1.14 m |
| 161 kV to 169 | 11 ft 8 in . | 3.56 m | 11 ft 8 in . | 3.56 m | 4 ft 3 in . | 1.29 m | 3 ft 9 in . |  |
| kV |  |  |  |  |  |  |  |  |
| $\begin{aligned} & 230 \mathrm{kV} \text { to } 242 \\ & \mathrm{kV} \end{aligned}$ | 13 ft 0 in. | 3.97 m | 13 ft 0 in. | 3.97 m | 5 ft 8 in . | 1.71 m | 5 ft 2 in . | 1.57 m |
|  |  |  |  |  |  |  |  |  |
| 345 kV to 362 | 15 ft 4 in. | 4.68 m | 15 ft 4 in . | 4.68 m | 9 ft 2 in . | 2.77 m | 8 ft 8 in . | 2.78 m |
| kV |  |  |  |  |  |  |  |  |
| 500 kV to 550 | 19 ft 0 in. | 5.8 m | 19 ft 0 in . | 5.8 m | 11 ft 10 in. | 3.61 m | 11 ft 4 in. | 3.54 m |
| kV |  |  |  |  |  |  |  |  |
| 765 kV to 800 | 23 ft 9 in. | 7.24 m | 23 ft 9 in . | 7.24 m | 15 ft 11 in. | 4.84 m | 15 ft 5 in. | 4.7 m |
| kV |  |  |  |  |  |  |  |  |

General Statement. Columns 1 through 5 of Table 130.2(C) all show various distances from the exposed energized electrical conductors or circuit part. They include dimensions that are added to a basic minimum air insulation distance. That basic minimum air insulation distance for voltages 72.5 kV and under are based on ANSI/IEEE 4-1995, Standard Techniques for High-Voltage Testing, Appendix 2B; and for voltages over 72.5 kV , are based on ANSI/IEEE 516-1995, Guide for Maintenance Methods on Energized Power Lines. These minimum air insulation distances required to avoid flashover are:

| Voltage | Minimum Air Insulation Distances |
| :--- | :--- |
| 300 V and less | 0 ft 0.03 in. |
| Over 300 V , not over 750 V | 0 ft 0.07 in. |
| Over 750 V , not over 2 kV | 0 ft 0.19 in. |
| Over 2 kV , not over 15 kV | 0 ft 1.5 in. |
| Over 15 kV , not over 36 kV | 0 ft 6.3 in. |
| Over 36 kV , not over 48.3 kV | 0 ft 10.0 in. |
| Over 48.3 kV , not over 72.5 kV | 1 ft 3.0 in. |
| Over 72.5 kV , not over 121 kV | 2 ft 1.2 in. |
| Over 138 kV , not over 145 kV | 2 ft 6.6 in. |
| Over 161 kV , not over 169 kV | 3 ft 0.0 in. |
| Over 230 kV , not over 242 kV | 4 ft 2.4 in. |
| Over 345 kV , not over 362 kV | 7 ft 5.8 in. |
| Over 500 kV , not over 550 kV | 10 ft 2.5 in. |
| Over 765 kV , not over 800 kV | 13 ft 10.3 in. |

Column No. 1 : The voltage ranges have been selected to group voltages that require similar approach distances based on the sum of the electrical withstand distance and an inadvertent movement factor. The value of the upper limit for a range is the maximum voltage for highest nominal voltage in the range based on ANSI C84.11995, Electric Power Systems and Equipment - Voltage Ratings (60 Hertz). For single-phase systems, select the range that is equal to the system's maximum phase-to-ground voltage times 1.732 .

Column No. 2: The distances in this column are based on OSHA's rule for unqualified persons to maintain a $10 \mathrm{ft}(3.05 \mathrm{~m})$ clearance for all voltages up to 50 kV (voltage-toground), plus 0.4 in . (102 mm) for each 1 kV over 50 kV .

Column No. 3: The distances are based on the following:
750 V and lower, use NEC Table 110-26(a) Working Clearances, Condition 2 for 151-600 V range.

For over 750 V , but not over 145 kV , use NEC Table 110-34(a) Working Space, Condition 2.

Over 145 kV , use OSHA's $10 \mathrm{ft}(3.05 \mathrm{~m})$ rules as used in Column No. 2.
Column No. 4: The distances are based on adding to the flashover dimensions shown above the following inadvertent movement distance:

300 V and less, avoid contact.

Based on experience and precautions for household 120/240 V systems.
Over 300 V and not over 750 V , add 1 ft 0 in. inadvertent movement.
These values have been found to be adequate over years of use in ANSI C2, National Electrical Safety Code, in the approach distances for supply workers.

Over 72.5 kV , add 1 ft 0 in . inadvertent movement.
These values have been found to be adequate over years of use in the National Electrical Safety Code in the approach distances for supply workers.

Column No. 5: The distances are based on the following:
300 V and less, avoid contact.
Over 300 but less than 750 V use NEC Table 230-51(c), Clearances.
Between open conductors and surfaces, 600 V not exposed to weather.
Over 750 V but not over 2.0 kV , value selected that fits in with adjacent values.
Over 2 kV but not over 72.5 kV, use NEC Table 490-24, Minimum Clearance of Live Parts, outdoor phase-to-ground values.

Over 72.5 kV , add 0 ft 6 in . inadvertent movement.
These values have been found to be adequate over years of use where there has been a hazard/risk analysis, either formal or informal, of a special work procedure that allows closer approach than that permitted by the restricted approach boundary distance.
17) Create the Arc Flash Hazard Warning Label

The Arc Flash Label lists important information such as Flash Hazard Boundary, Incident Energy at the given Working Distance, PPE clothing Hazard Risk Category (HRC), and the shock boundaries for Limited, Restricted, and Prohibited Approaches. An example of an arc flash warning label is shown below.


| Arc Flash and Shock Hazard |  |
| :---: | :---: |
| 5 Ft 5 ln | Flash Hazard Boundary |
| 9.9 | $\mathrm{cal} / \mathrm{cm}^{2}$ Flash Hazard at 1 Ft 6 In |
| Category 3 | FR Clothing Minimum Arc Rating of 25 (See NFPA 130.7(C)(10) for additional PPE) |
| 480 VAC | Shock Hazard when cover is removed |
| 00 | Glove Class |
| 3 Ft 6 ln | Limited Approach (Fixed Circuit) |
| 12 ln | Restricted Approach |
| 1 ln | Prohibited Approach |
| 03/17/2009 | Arc Flash Study Date IEEE 1584-2004a |
| Equipment ID (Name): | PNL-LP1B (PANEL LP1B) |
| Protective Device: | PNL LP1B FDR |

Scenario 2 - af with 2500kva xfmr
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Figure 2- Example Arc Flash Label

Figure 3 shows on the next page demonstrates how the four different protective boundaries are related and change depending upon the type of equipment, voltage rating, and incident energy used.

Limited Approach Boundary: An approach limit at a distance from an exposed live electrical conductor or circuit part within which a shock hazard exists. This value is determined by NFPA 70E (2009) Table 130.2(C).

Prohibited Approach Boundary: An approach limit at a distance from an exposed live electrical conductor or circuit part within which work is considered the same as making contact with the electrical conductor or circuit part. This value is determined by NFPA 70E (2009) Table 130.2(C).

Restricted Approach Boundary: An approach limit at a distance from an exposed live electrical conductor or circuit part within which there is an increased risk of shock, due to electrical arc over combined with inadvertent movement, for personnel working in close proximity to the energized electrical conductor or circuit part. This value is determined by NFPA 70E (2009) Table 130.2(C).

Arc Flash Boundary: When an arc flash hazard exists, an approach limit at a distance from a prospective arc source within which a person could receive a second degree burn if an electrical arc flash were to occur. This value is determined by the voltage,
type of equipment, and the time that the upstream protective device to clear the fault. The procedure is discussed in detail previously.

NFPA 70E (2209) Section130.3 Exception 1 states that an arc flash hazard analysis shall not be required where all of the following are met.

1. The circuit is rated 240 Volts or less
2. The circuit is supplied by one transformer
3. The transformer supplying the circuit is rated less than 125 kVA

For these locations, we assume that the Hazard Risk Category is 0 and we print labels stating as such. These labels also include the similar information as previously detailed and shown on the sample arc flash label.


Figure 3 - Arc Flash Boundary Relationship and Determination

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## Results

The arc flash calculations show that PPE clothing can be worn to increase personnel protection for most of the locations. Arc flash warning labels provided for these locations indicate the PPE required to be worn. The engineer recommends that the arc flash warning labels be installed on the electrical equipment to warn personnel of the potential hazard.

The following is a list of locations where the available incident energy exceeds 40 $\mathrm{Cal} / \mathrm{cm}^{\wedge} 2$. At these locations, the Required Protective FR Clothing Class is displayed as: "**** Dangerous!!! No FR Class Found. Before working on this equipment, the protection engineer strongly recommends that this equipment be de-energized.

## Maximum Arc Flash Energy (US) - Danger Only

## Scenario Descriptions <br> Scenario 1: Utility Power

## Calculation Details

IEEE 1584-2002/2004a Edition Bus + Line Side Report (Include Line Side + Load Side
Contributions), 80\% Cleared Fault Threshold, include Ind. Motors for 5.0 Cycles), mis-coordination checked

## Hazard Categories

Category 0: Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)
Category 1: FR Clothing Minimum Arc Rating of 4 (See NFPA 70E 130.7(C)(10) for additional PPE) Category 2: FR Clothing Minimum Arc Rating of 8 (See NFPA 70E 130.7(C)(10) for additional PPE)
Category 3: FR Clothing Minimum Arc Rating of 25 (See NFPA 70E 130.7(C)(10) for additional
PPE)
Category 4: FR Clothing Minimum Arc Rating of 40 (See NFPA 70E 130.7(C)(10) for additional
PPE)
DANGEROUS!: No PPE Exists - Do Not Work on Equipment while Energized!

## Arc Flash Notes

(*N1) Out of IEEE 1584 or NFPA 70E Ranges. LEE equation is used in this case and applicable for Open Air only. *N2) < 80\% Cleared Fault Threshold
*N3) Arcing Fault Current Low Tolerances Used
*N4) Equipment Specific Incident Energy and Flash Boundary Equations Used.
N5) Mis-coordinated, Upstream Device Tripped
(*N6) Special Instantaneous Protection in Use. Refer to Bus Detail \& Device Setting Sheets
*N7) Trip Time Unlinked with TCC.
*N8) Fault Current Unlinked with Fault Study results.
*N9) Max Arcing Duration Reached
*N10) Fuse Cable Protector Modeled.
N11) Out of IEEE 1584 Range, Lee Equation Used. Applicable for Open Air only. Existing Equipment type is not Open Air!
*N12) Out of IEEE 1584 Gap Range.
*N13) PPE up one Category
*N14) Zone Selective Interlock (ZSI) in Use.
*N15) Report as category 0 if fed by one transformer size < 125 kVA
*N16) Trip Time Recalculated
*N20) Out of NESC Voltage Range
*N21) Out of NESC Fault Current Range
N22) Out of NESC Max Clearing Range
(*N23) Out of NESC Voltage Range
*N24) Out of NESC Altitude Range
(*N25) Out of NESC Max Over Voltage Factor Range
(*N26) NESC SLG Fault is Zero

## Maximum Arc Flash Energy (US) - Danger Only

| Bus Name |  | Protective <br> Device <br> Name | Bus Volt (v) | Bus <br> Bolted Fault (kA) | Prot <br> Dev Bolted Fault (kA) | Prot <br> Dev Arcing Fault (kA) | Tripl Delay Time (sec) | Breaker Opening Time (sec) |  |  | $\begin{aligned} & 0 \\ & \frac{20}{0} \\ & 3 \\ & 3 \\ & \hline \end{aligned}$ | Arc Flash Bndry (in) | Work Dist (in) | Incident Energy (cal/cm2) | Required Protective Clothing Class |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15SWGR9001 (15SWGR9001) (315SWGR9001 MN LineSide) | 1 | 1-FDR TO 9001 | 480 | 28.65 | 28.13 | 15.82 | 2.00 | 0.000 | Y | PNL | 25 | 282 | 18 | 109.00 | Dangerous! (*N9) |
| 30SWBD9001 (30SWBD9001) (1230SWBD9001 MN LineSide) | 1 | 10-FDR TO 9002 | 480 | 30.59 | 30.51 | 17.00 | 2.00 | 0.000 | Y | PNL | 25 | 295 | 18 | 118.00 | Dangerous! (*N9) |
| 46SWGR9001 (46SWGR9001) (1846SWGR9001 MN LineSide) | 1 | 16-FDR TO 9004 | 480 | 35.43 | 35.30 | 19.25 | 2.00 | 0.000 | Y | PNL | 25 | 321 | 18 | 135.00 | Dangerous! (*N9) |

## Ways to Reduce Arc Flash Energy

There are many ways to reduce arc flash energies within a facility. The best method is to de-energize the equipment before work is performed. This reduces the energy level to zero and then arc flash hazard no longer exists.

In many locations, the obvious solution above can not be implemented. Many times, breakers must be racked in and out while the equipment is energized. Sometimes, it can be extremely hazardous or expensive to de-energize or shut down the equipment. For these locations and facilities, several methods are available to reduce the arc flash energy levels.

The three major factors that affect the amount of arc flash energy at a particular location are:

1. Device Operation Time - The time it takes for the upstream device to operate
2. Fault Current - The amount of fault current that will flow through the upstream protective device and is available at the fault location.
3. Working Distance - The amount of distance between the fault point and the worker.

It is the device operation time that effects the calculations the most, followed by fault current and working distance. In most cases, concentrating more on time reduction will result in a greater reduction in arc flash energy.

Many facilities use thermal magnetic trip units in their low voltage circuit breakers. These breakers have a fixed thermal and adjustable or fixed instantaneous function. Specifying breakers with solid state trip units using long, short, instantaneous, and ground fault functions will increase both equipment protection and coordination between devices. Tighter coordination between devices will mean a reduction in device operating times and arc flash energies.

For double ended substations using a bus tie, the mains and bus tie breaker settings can be set to the same settings. This enables the main to be set with a lower time delay which will reduce energy levels. Sacrificing the selective coordination between these devices is minor since most facilities rarely close the bus tie breakers except for maintenance purposes.

Most modern low voltage switchboards or switchgear can be equipped with trip units that are zone interlocked. If a fault occurs on the main bus, then the main and tie breakers will trip instantaneously instead of using the normal delayed coordination settings.

New trip units are being manufactured with maintenance switches. When this trip unit is switched to maintenance mode, a low instantaneous function is enabled. Should a fault occur, the breaker will quickly trip and reduce the arc flash hazard downstream. These trip units are available on new breakers or retrofit kits for old style power circuit breakers.

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Medium voltage relay operating times can be reduced using some of the same techniques used above for low voltage switchgear. The operating (trip) times can sometimes be reduced by changing the relay operating curve. These times can also be changed by reducing the selective coordination safety margin and by selecting a lower time dial setting.

Many newer protective relays have group settings. This allows the relay settings to change depending upon an input to the relay. A maintenance switch can be added and connected to the input of one of the relays. When the switch is turned to the on position, it tells the relay to use a lower set of relay settings. Should a fault occur downstream from the relay, the relay will trip sooner and reduce the arc flash energy.

Arc flash energy can also be reduced by modification of the work procedures. Examples of this are listed below:

1. Eliminating paralleling of transformers (reduces fault current and arc flash energy)
2. Eliminating work between Transformer Secondary and Main Breaker. (Normally, the primary device must sense the fault on the secondary side of the transformer. This lower level of fault current, seen by the primary devices causes the trip time to be long. This increased trip time means larger energy levels.
3. Implementing faster trip times for maintenance work (See descriptions in previous section)
a) Circuit Breakers
b) Relays
c) Using infrared windows for infrared surveys
d) Working at a greater distance
e) Do not stand in front of electrical equipment when operating or inserting (racking in).
f) Remote breaker racking

Arc Flash hazards exist in every facility. This hazard can be reduced by reviewing types of equipment used, device operation times, and working distance. Each location must be analyzed and the best engineered solution determined. In summary, Arc Flash Energy can be reduced by increasing the worker distance, reducing fault currents, and decreasing the trip times.

TAB 12

## Maximum Arc Flash Energy (US) - All

## Scenario Descriptions <br> Scenario 1: Utility Power

## Calculation Details

IEEE 1584-2002/2004a Edition Bus + Line Side Report (Include Line Side + Load Side
Contributions), 80\% Cleared Fault Threshold, include Ind. Motors for 5.0 Cycles), mis-coordination checked

## Hazard Categories

Category 0: Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)
Category 1: FR Clothing Minimum Arc Rating of 4 (See NFPA 70E 130.7(C)(10) for additional PPE) Category 2: FR Clothing Minimum Arc Rating of 8 (See NFPA 70E 130.7(C)(10) for additional PPE)
Category 3: FR Clothing Minimum Arc Rating of 25 (See NFPA 70E 130.7(C)(10) for additional
PPE)
Category 4: FR Clothing Minimum Arc Rating of 40 (See NFPA 70E 130.7(C)(10) for additional
PPE)
DANGEROUS!: No PPE Exists - Do Not Work on Equipment while Energized!

## Arc Flash Notes

(*N1) Out of IEEE 1584 or NFPA 70E Ranges. LEE equation is used in this case and applicable for Open Air only.
*N2) < 80\% Cleared Fault Threshold
*N3) Arcing Fault Current Low Tolerances Used
*N4) Equipment Specific Incident Energy and Flash Boundary Equations Used.
N5) Mis-coordinated, Upstream Device Tripped.
(*N6) Special Instantaneous Protection in Use. Refer to Bus Detail \& Device Setting Sheets
*N7) Trip Time Unlinked with TCC.
(*N8) Fault Current Unlinked with Fault Study results.
*N9) Max Arcing Duration Reached
*N10) Fuse Cable Protector Modeled.
*N11) Out of IEEE 1584 Range, Lee Equation Used. Applicable for Open Air only. Existing Equipment type is not Open Air!
*N12) Out of IEEE 1584 Gap Range.
*N13) PPE up one Category
*N14) Zone Selective Interlock (ZSI) in Use.
*N15) Report as category 0 if fed by one transformer size < 125 kVA
*N16) Trip Time Recalculated
N20) Out of NESC Voltage Range
*N21) Out of NESC Fault Current Range
N22) Out of NESC Max Clearing Range
(*N23) Out of NESC Voltage Range
*N24) Out of NESC Altitude Range
(*N25) Out of NESC Max Over Voltage Factor Range
(*N26) NESC SLG Fault is Zero

Maximum Arc Flash Energy (US) - All

| Bus Name |  | Protective Device Name | Bus Volt <br> (v) | Bus <br> Bolted Fault (kA) | Prot <br> Dev Bolted Fault (kA) | Prot <br> Dev Arcing Fault (kA) | Tripl Delay Time (sec) | Breaker Opening Time (sec) | $\begin{aligned} & \text { Q } \\ & 0 \\ & 0 \\ & 0 \\ & \hline 2 \end{aligned}$ |  | $\begin{aligned} & 0 \\ & \frac{2}{0} \\ & \frac{3}{3} \\ & \hline \end{aligned}$ | Arc <br> Flash Bndry (in) | Work Dist (in) | Incident Energy (cal/cm2) | Required Protective Clothing Class |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10DP9201 (10DP9201) | 1 | FDR TO 10DP9201 | 480 | 22.01 | 22.01 | 12.86 | 0.01 | 0.000 | Y | PNL | 25 | 10 | 18 | 0.44 | Category 0 |
| 10DP9201 (10DP9201) (10DP9201 MAIN LineSide) | 1 | FDR TO 10DP9201 | 480 | 22.01 | 22.01 | 12.86 | 0.01 | 0.000 | Y | PNL | 25 | 10 | 18 | 0.44 | Category 0 |
| 10LP9201 (10LP9201) | 1 | FDR TO 10XFMR9201 | 208 | 1.03 | 1.03 | 0.88 | 2.00 | 0.000 | Y | PNL | 25 | 18 | 18 | 1.20 | Category 0 (*N9) (*N15) |
| 10SWBD9101 (10SWBD9101) | 1 | 4-FDR TO 10SWBD91 | 480 | 25.86 | 25.86 | 12.55 | 0.17 | 0.000 | Y | PNL | 25 | 54 | 18 | 7.20 | Category 2 (*N3) |
| 10VFD1001 (10VFD1001) | 1 | 5-FDR TO 10P1001 | 480 | 24.19 | 24.19 | 13.95 | 0.01 | 0.000 | $Y$ | PNL | 25 | 13 | 18 | 0.70 | Category 0 |
| 10VFD1002 (10VFD1002) | 1 | FDR TO 10P1002 | 480 | 24.19 | 24.19 | 13.95 | 0.01 | 0.000 | Y | PNL | 25 | 13 | 18 | 0.70 | Category 0 |
| 10VFD1003 (10VFD1003) | 1 | FDR TO 10P1003 | 480 | 24.19 | 24.19 | 13.95 | 0.01 | 0.000 | Y | PNL | 25 | 13 | 18 | 0.70 | Category 0 |
| 10XFMR9201P (10XFMR9201 PRI) | 1 | FDR TO 10DP9201 | 480 | 16.99 | 16.99 | 10.31 | 0.01 | 0.000 | Y | PNL | 25 | 8 | 18 | 0.34 | Category 0 (*N5) |
| 10XFMR9201S (10XFMR9201 SEC) | 1 | FDR TO 10XFMR9201 | 208 | 1.05 | 1.05 | 0.89 | 2.00 | 0.000 | Y | PNL | 25 | 18 | 18 | 1.20 | Category 0 (*N9) (*N15) |
| 15SWGR9001 (15SWGR9001) | 1 | 3-15SWGR9001 MN | 480 | 28.65 | 28.13 | 15.82 | 0.28 | 0.000 | Y | PNL | 25 | 85 | 18 | 15.00 | Category 3 |
| 15SWGR9001 (15SWGR9001) (315SWGR9001 MN LineSide) | 1 | 1-FDR TO 9001 | 480 | 28.65 | 28.13 | 15.82 | 2.00 | 0.000 | Y | PNL | 25 | 282 | 18 | 109.00 | Dangerous! (*N9) |
| 20DP9201 (20DP9201) | 1 | FDR TO 20DP9201 | 480 | 16.06 | 16.06 | 9.83 | 0.01 | 0.000 | $Y$ | PNL | 25 | 10 | 18 | 0.45 | Category 0 |
| $20 \mathrm{LP9201} \mathrm{(20LP9201)}$ | 1 | FDR TO 20XFMR9201 | 208 | 1.02 | 1.02 | 0.88 | 2.00 | 0.000 | Y | PNL | 25 | 18 | 18 | 1.20 | Category 0 (*N9) (*N15) |
| 20MCC9101 (20MCC9101) | 1 | 8-FDR TO 20MCC9101 | 480 | 25.55 | 25.03 | 14.32 | 0.05 | 0.000 | Y | PNL | 25 | 26 | 18 | 2.30 | Category 1 |
| 20XFMR9201P (20XFMR9201 PRI) | 1 | FDR TO 20DP9201 | 480 | 12.57 | 12.57 | 7.97 | 0.01 | 0.000 | $Y$ | PNL | 25 | 9 | 18 | 0.37 | Category 0 (*N5) |
| 20XFMR9201S (20XFMR9201 SEC) | 1 | FDR TO 20XFMR9201 | 208 | 1.04 | 1.04 | 0.89 | 2.00 | 0.000 | Y | PNL | 25 | 18 | 18 | 1.20 | Category 0 (*N9) (*N15) |
| 30DP9201 (30DP9201) | 1 | FDR TO 30DP9201 | 480 | 13.02 | 13.02 | 8.21 | 0.01 | 0.000 | Y | PNL | 25 | 7 | 18 | 0.27 | Category 0 |
| 30LP9201 (30LP9201) | 1 | FDR TO 30XFMR9201 | 208 | 1.01 | 1.01 | 0.87 | 2.00 | 0.000 | Y | PNL | 25 | 18 | 18 | 1.20 | Category 0 (*N9) (*N15) |
| 30MCC9101 (30MCC9101) | 1 | FDR TO 30MCC9101 | 480 | 25.99 | 25.92 | 14.79 | 0.01 | 0.000 | Y | PNL | 25 | 11 | 18 | 0.51 | Category 0 |
| 30MTS8601 (30MTS8601) | 1 | FDR TO 30MTS8601 | 480 | 28.22 | 28.22 | 15.91 | 0.01 | 0.000 | Y | PNL | 25 | 14 | 18 | 0.75 | Category 0 |
| 30SWBD9001 (30SWBD9001) | 1 | 12-30SWBD9001 MN | 480 | 30.59 | 30.51 | 17.00 | 0.17 | 0.000 | Y | PNL | 25 | 66 | 18 | 10.00 | Category 3 |
| 30SWBD9001 (30SWBD9001) (1230SWBD9001 MN LineSide) | 1 | 10-FDR TO 9002 | 480 | 30.59 | 30.51 | 17.00 | 2.00 | 0.000 | Y | PNL | 25 | 295 | 18 | 118.00 | Dangerous! (*N9) |
| 30VFD1001 (30VFD1001) | 1 | 13-FDR TO 30VFD100 | 480 | 29.35 | 29.35 | 16.45 | 0.02 | 0.000 | Y | PNL | 25 | 18 | 18 | 1.20 | Category 1 |
| 30VFD1002 (30VFD1002) | 1 | FDR TO 30VFD1002 | 480 | 29.35 | 29.35 | 16.45 | 0.02 | 0.000 | Y | PNL | 25 | 18 | 18 | 1.20 | Category 1 |
| 30VFD7600 (30VFD7600) | 1 | FDR TO 30VFD7600 | 480 | 28.22 | 28.22 | 15.91 | 0.01 | 0.000 | Y | PNL | 25 | 14 | 18 | 0.75 | Category 0 |
| 30VFD8601 (30VFD8601) | 1 | FDR TO 30MTS8601 | 480 | 25.50 | 25.50 | 14.59 | 0.01 | 0.000 | Y | PNL | 25 | 13 | 18 | 0.71 | Category 0 |
| 30XFMR9201P (30XFMR9201 PRI) | 1 | FDR TO 30DP9201 | 480 | 10.61 | 10.61 | 6.90 | 0.01 | 0.000 | Y | PNL | 25 | 6 | 18 | 0.22 | Category 0 (*N5) |
| 30XFMR9201S (30XFMR9201 SEC) | 1 | FDR TO 30XFMR9201 | 208 | 1.03 | 1.03 | 0.88 | 2.00 | 0.000 | Y | PNL | 25 | 18 | 18 | 1.20 | Category 0 (*N9) (*N15) |
| 40DP9201 (40DP9201) | 1 | FDR TO 40DP9201 | 480 | 26.42 | 26.42 | 15.04 | 0.01 | 0.000 | Y | PNL | 25 | 11 | 18 | 0.52 | Category 0 |
| 40DP9202 (40DP9202) | 1 | FDR TO 40DP9202 | 480 | 11.43 | 11.43 | 7.35 | 0.01 | 0.000 | Y | PNL | 25 | 7 | 18 | 0.24 | Category 0 |
| 40LP9201 (40LP9201) | 1 | FDR TO 40XFMR9201 | 208 | 1.03 | 1.03 | 0.88 | 2.00 | 0.000 | $Y$ | PNL | 25 | 18 | 18 | 1.20 | Category 0 (*N9) (*N15) |
| 40LP9202 (40LP9202) | 1 | FDR TO 40XFMR9202 | 208 | 1.01 | 1.01 | 0.87 | 2.00 | 0.000 | $Y$ | PNL | 25 | 18 | 18 | 1.20 | Category 0 (*N9) (*N15) |
| 40MCC9201 (40MCC9201) | 1 | 27-FDR TO 40MCC920 | 480 | 21.65 | 21.54 | 12.62 | 0.03 | 0.000 | Y | PNL | 25 | 19 | 18 | 1.40 | Category 1 |
| 40SWBD9101 (40SWBD9101) | 1 | 26-FDR TO 40SWBD9 | 480 | 33.45 | 33.32 | 18.32 | 0.05 | 0.000 | Y | PNL | 25 | 31 | 18 | 2.90 | Category 1 |

Maximum Arc Flash Energy (US) - All

| Bus Name | の D 0 0 0 0 | Protective Device Name | Bus Volt <br> (v) | Bus <br> Bolted Fault (kA) | Prot <br> Dev Bolted Fault (kA) | Prot <br> Dev Arcing Fault (kA) | Trip/ Delay Time (sec) | Breaker Opening Time (sec) | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & \\ & \hline 2 \end{aligned}$ |  | $\begin{aligned} & 0 \\ & 00 \\ & 3 \\ & 3 \\ & \hline 3 \end{aligned}$ | Arc Flash Bndry (in) | Work Dist (in) | Incident Energy (cal/cm2) | Required Protective Clothing Class |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 40XFMR9201P (40XFMR9201 PRI) | 1 | FDR TO 40DP9201 | 480 | 19.23 | 19.23 | 11.46 | 0.01 | 0.000 | Y | PNL | 25 | 9 | 18 | 0.38 | Category 0 (*N5) |
| 40XFMR9201S (40XFMR9201 SEC) | 1 | FDR TO 40XFMR9201 | 208 | 1.05 | 1.05 | 0.90 | 2.00 | 0.000 | $Y$ | PNL | 25 | 18 | 18 | 1.20 | Category 0 (*N9) (*N15) |
| 40XFMR9202P (40XFMR9202 PRI) | 1 | FDR TO 40DP9202 | 480 | 9.47 | 9.47 | 6.26 | 0.01 | 0.000 | $Y$ | PNL | 25 | 6 | 18 | 0.20 | Category 0 (*N5) |
| 40XFMR9202S (40XFMR9202 SEC) | 1 | FDR TO 40XFMR9202 | 208 | 1.03 | 1.03 | 0.88 | 2.00 | 0.000 | $Y$ | PNL | 25 | 18 | 18 | 1.20 | Category 0 (*N9) (*N15) |
| 45VFD1001 (45VFD1001) | 1 | 20-FDR TO 45VFD100 | 480 | 32.07 | 32.07 | 17.74 | 0.02 | 0.000 | $Y$ | PNL | 25 | 19 | 18 | 1.30 | Category 1 |
| 45VFD1003 (45VFD1003) | 1 | FDR TO 45VFD1003 | 480 | 32.07 | 32.07 | 17.74 | 0.02 | 0.000 | $Y$ | PNL | 25 | 19 | 18 | 1.30 | Category 1 |
| 45VFD1006 (45VFD1006) | 1 | 23-FDR TO 45VFD100 | 480 | 26.58 | 26.58 | 15.12 | 0.02 | 0.000 | Y | PNL | 25 | 16 | 18 | 0.95 | Category 0 |
| 45VFD1007 (45VFD1007) | 1 | FDR TO 45VFD1007 | 480 | 25.48 | 25.48 | 14.58 | 0.02 | 0.000 | $Y$ | PNL | 25 | 15 | 18 | 0.93 | Category 0 |
| 46SWBD9101 (46SWBD9101) | 1 | 19-FDR TO 46SWBD9 | 480 | 33.78 | 33.78 | 18.55 | 0.17 | 0.000 | Y | PNL | 25 | 70 | 18 | 11.00 | Category 3 |
| 46SWGR9001 (46SWGR9001) | 1 | 18-46SWGR9001 MN | 480 | 35.43 | 35.30 | 19.25 | 0.28 | 0.000 | $Y$ | PNL | 25 | 97 | 18 | 19.00 | Category 3 |
| 46SWGR9001 (46SWGR9001) (1846SWGR9001 MN LineSide) | 1 | 16-FDR TO 9004 | 480 | 35.43 | 35.30 | 19.25 | 2.00 | 0.000 | Y | PNL | 25 | 321 | 18 | 135.00 | Dangerous! (*N9) |
| 50DP9201 (50DP9201) | 1 | FDR TO 50DP9201 | 480 | 10.53 | 10.53 | 6.85 | 0.01 | 0.000 | Y | PNL | 25 | 8 | 18 | 0.29 | Category 0 |
| 50DP9201 (50DP9201) (50DP9201 MAIN LineSide) | 1 | FDR TO 50DP9201 | 480 | 10.53 | 10.53 | 6.85 | 0.01 | 0.000 | Y | PNL | 25 | 8 | 18 | 0.29 | Category 0 |
| 50LP9201 (50LP9201) | 1 | FDR TO 50XFMR9201 | 208 | 1.95 | 1.95 | 1.38 | 2.00 | 0.000 | Y | PNL | 25 | 18 | 18 | 1.20 | Category 0 (*N9) (*N15) |
| 50LP9202 (50LP9202) | 1 | FDR TO 50XFMR9201 | 208 | 1.87 | 1.87 | 1.34 | 2.00 | 0.000 | $Y$ | PNL | 25 | 18 | 18 | 1.20 | Category 0 (*N9) (*N15) |
| 50XFMR9201P (50XFMR9201 PRI) | 1 | FDR TO 50DP9201 | 480 | 9.84 | 9.84 | 6.47 | 0.01 | 0.000 | Y | PNL | 25 | 7 | 18 | 0.28 | Category 0 (*N5) |
| 50XFMR9201S (50XFMR9201 SEC) | 1 | FDR TO 50XFMR9201 | 208 | 1.97 | 1.97 | 1.39 | 2.00 | 0.000 | $Y$ | PNL | 25 | 18 | 18 | 1.20 | Category 0 (*N9) (*N15) |
| 70DP9201 (70DP9201) | 1 | 70DP9201 MAIN | 480 | 7.86 | 7.86 | 5.34 | 0.01 | 0.000 | Y | PNL | 25 | 7 | 18 | 0.25 | Category 0 |
| 70DP9201 (70DP9201) (70DP9201 MAIN LineSide) | 1 | FDR TO 70DP9201 | 480 | 7.86 | 7.86 | 4.54 | 0.02 | 0.000 | Y | PNL | 25 | 7 | 18 | 0.28 | Category 0 (*N3) |
| $70 \mathrm{LP9201}$ (70LP9201) | 1 | FDR TO 70XFMR9201 | 208 | 1.90 | 1.90 | 1.35 | 1.15 | 0.000 | Y | PNL | 25 | 18 | 18 | 1.20 | Category 0 (*N15) |
| 70LP9202 (70LP9202) | 1 | FDR TO 70XFMR9202 | 208 | 1.90 | 1.90 | 1.35 | 1.15 | 0.000 | Y | PNL | 25 | 18 | 18 | 1.20 | Category 0 (*N15) |
| 70XFMR9201P (70XFMR9201 PRI) | 1 | 70DP9201 MAIN | 480 | 7.46 | 7.46 | 5.11 | 0.01 | 0.000 | Y | PNL | 25 | 7 | 18 | 0.25 | Category 0 (*N5) |
| 70XFMR9201S (70XFMR9201 SEC) | 1 | FDR TO 70XFMR9201 | 208 | 1.92 | 1.92 | 1.37 | 1.13 | 0.000 | Y | PNL | 25 | 18 | 18 | 1.20 | Category 0 (*N15) |
| 70XFMR9202P (70XFMR9202 PRI) | 1 | 70DP9201 MAIN | 480 | 7.46 | 7.46 | 5.11 | 0.01 | 0.000 | Y | PNL | 25 | 7 | 18 | 0.25 | Category 0 (*N5) |
| 70XFMR9202S (70XFMR9202 SEC) | 1 | FDR TO 70XFMR9202 | 208 | 1.92 | 1.92 | 1.37 | 1.13 | 0.000 | Y | PNL | 25 | 18 | 18 | 1.20 | Category 0 (*N15) |

TAB 13

## Arc Flash Label Installation Instructions

1) Before applying the labels to the equipment, read the important information listed below.
2) Always clean the surface with detergent to remove all grease and dirt. Wipe surface dry before applying the label.
3) Where possible, apply labels at eye level on equipment covers
4) The labels are CUSTOM MADE and are specific for each piece of electrical equipment. Each label has an alpha-numeric ID and Name. The name is shown in parenthesis. Care must be taken when attaching the labels to the equipment.
a) VERIFY THAT YOU ARE ATTACHING THE CORRECT LABEL TO THE EQUIPMENT!!!
b) If you are unsure, please contact our office immediately at 253-639-8535.
5) Some locations will have a Line Side Label and a bus label. They should be installed at locations where maintenance staff could be exposed to energized parts on the line side of a fuse or circuit breaker. Examples of this are Main Breakers in Panelboard, Switchboards, Motor Control Centers and Switchgear. Bus labels are for the main bus of the equipment and are located downstream from the main breaker (if the main breaker exists). Both the bus ID and name will be the same. The difference is that a line side label will state, Line Side 6-DBA MAIN
a) Attach the line side label at the main breaker line side. Usually this is located on the top of the main breaker but please verify before attaching the label.
b) Attach the bus label downstream from the main breaker.


Figure 4 - Example of Bus Side Label


Figure 5 - Example of Line Side of a Protective Device
6) Transformers will have two labels provided. One label will be for the primary and the other label for the secondary. Place the labels on the appropriate ends (or sides) of the transformer. If the transformer is a small distribution type (i.e. $480 / 208 \mathrm{~V}$ ) place both the primary and secondary labels on the front of the transformer.
7) Locations where the label will be exposed to direct sun light should be brought to the attention of PowerStudies.com. We will provide a special UV resistant label.

## Arc Flash and Shock Hazard

0 Ft 10 In
0.44

Category 0
Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Shock Hazard when cover is removed
Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 10DP9201 (10DP9201)
FDR TO 10DP9201

Scenario 1 - Utility Power
Study Performed By PowerStudies.com (253) 639-8535

## WARNING

## Arc Flash and Shock Hazard

## 1 Ft 6 In <br> 1.2

Category 0

208 VAC
00
3 Ft 6 In
Avoid Contact
Avoid Contact
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary
cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 10LP9201 (10LP9201)
FDR TO 10XFMR9201

Scenario 1-Utility Power

## WARNING

## Arc Flash and Shock Hazard

0 Ft 10 In
0.44

Category 0

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:
Line Side of:

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Scenario 1 - Utility Power Study Performed By PowerStudies.com (253) 639-8535


Arc Flash and Shock Hazard

0 Ft 8 In
0.34

Category 0

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary
cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In
Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 10XFMR9201P (10XFMR9201 PRI) FDR TO 10DP9201

Scenario 1-Utility Power

[^1]
## Arc Flash and Shock Hazard

## 1 Ft 6 In <br> 1.2

Category 0
Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

208 VAC
00
3 Ft 6 In
Avoid Contact
Avoid Contact 04/28/2011
Equipment ID (Name):
Protective Device:

Shock Hazard when cover is removed
Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 10XFMR9201S (10XFMR9201 SEC) FDR TO 10XFMR9201

Scenario 1-Utility Power

## WARNING

## Arc Flash and Shock Hazard

## 1 Ft 6 In

1.2

Category 0

208 VAC
00
3 Ft 6 In
Avoid Contact
Avoid Contact
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary
cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 20LP9201 (20LP9201)
FDR TO 20XFMR9201

Scenario 1-Utility Power

## WARNING

## Arc Flash and Shock Hazard

0 Ft 10 In
0.45

Category 0

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 20DP9201 (20DP9201) FDR TO 20DP9201

Scenario 1-Utility Power


Arc Flash and Shock Hazard

0 Ft 9 In
0.37

Category 0

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 20XFMR9201P (20XFMR9201 PRI) FDR TO 20DP9201

Scenario 1-Utility Power

## Arc Flash and Shock Hazard

## 1 Ft 6 In <br> 1.2

Category 0
Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

208 VAC
00
3 Ft 6 In
Avoid Contact
Avoid Contact 04/28/2011
Equipment ID (Name):
Protective Device:

Shock Hazard when cover is removed
Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 20XFMR9201S (20XFMR9201 SEC) FDR TO 20XFMR9201

Scenario 1-Utility Power

## WARNING

## Arc Flash and Shock Hazard

1 Ft 6 In
1.2

Category 0

208 VAC
00
3 Ft 6 In
Avoid Contact
Avoid Contact
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 30LP9201 (30LP9201)
FDR TO 30XFMR9201

Scenario 1-Utility Power

## WARNING

## Arc Flash and Shock Hazard

0 Ft 7 In
0.27

Category 0

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 30DP9201 (30DP9201) FDR TO 30DP9201

Scenario 1-Utility Power


Arc Flash and Shock Hazard

0 Ft 11 In
0.51

Category 0

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 30MCC9101 (30MCC9101)
FDR TO 30MCC9101

Scenario 1 - Utility Power

## Arc Flash and Shock Hazard

1 Ft 2 ln
0.75
Category 0

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

480 VAC
00
3 Ft 6 In
12 In
Shock Hazard when cover is removed
Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
1 ln
04/28/2011
Equipment ID (Name):
Protective Device:
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 30MTS8601 (30MTS8601)
FDR TO 30MTS8601

Scenario 1-Utility Power
Study Performed By PowerStudies.com (253) 639-8535

## WARNING

## Arc Flash and Shock Hazard

1 Ft 6 In
1.2

Category 0

208 VAC
00
3 Ft 6 In
Avoid Contact
Avoid Contact
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 30XFMR9201S (30XFMR9201 SEC) FDR TO 30XFMR9201

Scenario 1-Utility Power

## Arc Flash and Shock Hazard

0 Ft 6 In
0.22

Category 0

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 30XFMR9201P (30XFMR9201 PRI) FDR TO 30DP9201

Scenario 1-Utility Power


Arc Flash and Shock Hazard

0 Ft 11 In
0.52

Category 0

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 40DP9201 (40DP9201)
FDR TO 40DP9201

Scenario 1 - Utility Power

## Arc Flash and Shock Hazard

0 Ft 7 In

$$
0.24
$$

Category 0
Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

480 VAC 00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:
Shock Hazard when cover is removed

## Glove Class

Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 40DP9202 (40DP9202)
FDR TO 40DP9202

Scenario 1-Utility Power
Study Performed By PowerStudies.com (253) 639-8535

## MA PAN

## Arc Flash and Shock Hazard

$$
1 \text { Ft } 6 \text { In }
$$

$$
1.2
$$

Category 0
208 VAC
00
3 Ft 6 In
Avoid Contact
Avoid Contact
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 40LP9202 (40LP9202) FDR TO 40XFMR9202

Scenario 1 - Utility Power

## WARNING

## Arc Flash and Shock Hazard

1 Ft 6 In
1.2

Category 0
208 VAC
00
3 Ft 6 In
Avoid Contact
Avoid Contact
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 40LP9201 (40LP9201)
FDR TO 40XFMR9201

Scenario 1-Utility Power Study Performed By PowerStudies.com (253) 639-8535


Arc Flash and Shock Hazard

1 Ft 7 In
1.4

Category 1
480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary
cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In
FR Clothing Minimum Arc Rating of 4 (See NFPA 70E 130.7(C)(10) for additional PPE)
Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 40MCC9201 (40MCC9201)
27-FDR TO 40MCC9201

Scenario 1-Utility Power

## Arc Flash and Shock Hazard

0 Ft 9 In 0.38

Category 0
Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

480 VAC 00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:
Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 40XFMR9201P (40XFMR9201 PRI) FDR TO 40DP9201

Scenario 1 - Utility Power
Study Performed By PowerStudies.com (253) 639-8535

## WARNING

## Arc Flash and Shock Hazard

0 Ft 6 In
0.2

Category 0

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary
cal/cm² Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 40XFMR9202P (40XFMR9202 PRI) FDR TO 40DP9202

## WARNING

## Arc Flash and Shock Hazard

1 Ft 6 In
1.2

Category 0

208 VAC
00
3 Ft 6 In
Avoid Contact
Avoid Contact
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm² Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach Arc Flash Study Date IEEE 1584-2004a 40XFMR9201S (40XFMR9201 SEC) FDR TO 40XFMR9201

Scenario 1-Utility Power


Arc Flash and Shock Hazard

1 Ft 6 In
1.2

Category 0

208 VAC
00
3 Ft 6 In
Avoid Contact
Avoid Contact
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm² Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 40XFMR9202S (40XFMR9202 SEC) FDR TO 40XFMR9202

Scenario 1-Utility Power

[^2]
## Arc Flash and Shock Hazard

0 Ft 8 ln
0.29
0.29

Category 0
Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:
Shock Hazard when cover is removed
Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 50DP9201 (50DP9201)
FDR TO 50DP9201

Scenario 1-Utility Power
Study Performed By PowerStudies.com (253) 639-8535

## MA PANM

## Arc Flash and Shock Hazard

$$
1 \text { Ft } 6 \text { In }
$$

1.2

Category 0

208 VAC
00
3 Ft 6 In
Avoid Contact
Avoid Contact
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 50LP9201 (50LP9201) FDR TO 50XFMR9201

Scenario 1-Utility Power

## WARNING

## Arc Flash and Shock Hazard

0 Ft 8 In
0.29

Category 0

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:
Line Side of:

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Scenario 1 - Utility Power Study Performed By PowerStudies.com (253) 639-8535


## WARNING

Arc Flash and Shock Hazard

1 Ft 6 In
1.2

Category 0

208 VAC
00
3 Ft 6 In
Avoid Contact
Avoid Contact
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary
cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In
Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 50LP9202 (50LP9202)
FDR TO 50XFMR9201

Scenario 1-Utility Power

## Arc Flash and Shock Hazard

0 Ft 7 In

$$
0.28
$$

Category 0
Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

480 VAC 00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:
Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 50XFMR9201P (50XFMR9201 PRI) FDR TO 50DP9201

Scenario 1-Utility Power
Study Performed By PowerStudies.com (253) 639-8535

## WARNING

## Arc Flash and Shock Hazard

0 Ft 7 In
0.25

Category 0
480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary
cal/cm² Flash Hazard at 1 Ft 6 In
Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 70DP9201 (70DP9201) 70DP9201 MAIN

Scenario 1-Utility Power
Study Performed By PowerStudies.com (253) 639-8535

## WARNING

## Arc Flash and Shock Hazard

1 Ft 6 In
1.2

Category 0

208 VAC
00
3 Ft 6 In
Avoid Contact
Avoid Contact
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm² Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach Arc Flash Study Date IEEE 1584-2004a 50XFMR9201S (50XFMR9201 SEC) FDR TO 50XFMR9201

Scenario 1-Utility Power


Arc Flash and Shock Hazard

0 Ft 7 In
0.28

Category 0

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:
Line Side of:
Scenario 1-Utility Power
Study Performed By PowerStudies.com (253) 639-8535

## Arc Flash and Shock Hazard

## 1 Ft 6 In <br> 1.2

Category 0

208 VAC
00
3 Ft 6 In
Avoid Contact
Avoid Contact 04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed
Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 70LP9201 (70LP9201) FDR TO 70XFMR9201

Scenario 1 - Utility Power
Study Performed By PowerStudies.com (253) 639-8535

## WARNING

## Arc Flash and Shock Hazard

0 Ft 7 In
0.25

Category 0

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary
cal/ $\mathrm{cm}^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 70XFMR9201P (70XFMR9201 PRI) 70DP9201 MAIN

Scenario 1 - Utility Power

## WARNING

## Arc Flash and Shock Hazard

1 Ft 6 In
1.2

Category 0

208 VAC
00
3 Ft 6 In
Avoid Contact
Avoid Contact
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 70LP9202 (70LP9202) FDR TO 70XFMR9202

Scenario 1-Utility Power Study Performed By PowerStudies.com (253) 639-8535


Arc Flash and Shock Hazard

1 Ft 6 In
1.2

Category 0

208 VAC
00
3 Ft 6 In
Avoid Contact
Avoid Contact
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 70XFMR9201S (70XFMR9201 SEC) FDR TO 70XFMR9201

Scenario 1-Utility Power

## Arc Flash and Shock Hazard

0 Ft 7 In
0.25

Category 0
Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

480 VAC 00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Shock Hazard when cover is removed
Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 70XFMR9202P (70XFMR9202 PRI) 70DP9201 MAIN

Scenario 1-Utility Power
Study Performed By PowerStudies.com (253) 639-8535

## WARNING

## Arc Flash and Shock Hazard

## 4 Ft 6 In <br> 7.2

Category 2

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary
cal/cm² Flash Hazard at 1 Ft 6 In FR Clothing Minimum Arc Rating of 8 (See NFPA 70E 130.7(C)(10) for additional PPE)
Shock Hazard when cover is removed

## Glove Class

Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 10SWBD9101 (10SWBD9101) 4-FDR TO 10SWBD9101

Scenario 1-Utility Power

## WARNING

## Arc Flash and Shock Hazard

1 Ft 6 In
1.2

Category 0

208 VAC
00
3 Ft 6 In
Avoid Contact
Avoid Contact
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach Arc Flash Study Date IEEE 1584-2004a 70XFMR9202S (70XFMR9202 SEC) FDR TO 70XFMR9202

Scenario 1-Utility Power


Arc Flash and Shock Hazard

1 Ft 1 In
0.7

Category 0
480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 10VFD1001 (10VFD1001)
5-FDR TO 10 P 1001

Scenario 1-Utility Power

## Arc Flash and Shock Hazard

1 Ft 1 In
0.7
0.7

Category 0
Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:
Shock Hazard when cover is removed
Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 10VFD1002 (10VFD1002)
FDR TO 10P1002

Scenario 1-Utility Power
Study Performed By PowerStudies.com (253) 639-8535

## WARNING

## Arc Flash and Shock Hazard

7 Ft 1 In
15
Category 3
480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary
cal/ $\mathrm{cm}^{2}$ Flash Hazard at 1 Ft 6 In
FR Clothing Minimum Arc Rating of 25 (See NFPA 70E 130.7(C)(10) for additional PPE)
Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 15SWGR9001 (15SWGR9001) 3-15SWGR9001 MN

Scenario 1-Utility Power

## WARNING

## Arc Flash and Shock Hazard

1 Ft 1 In
0.7

Category 0

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:
Scenario 1-Utility Power Study Performed By PowerStudies.com (253) 639-8535


## Arc Flash and Shock Hazard

23 Ft 6 In
109
Dangerous!

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:
Line Side of:
Scenario 1-Utility Power
Study Performed By PowerStudies.com (253) 639-8535

## Arc Flash and Shock Hazard

2 Ft 2 In
2.3

Category 1

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In FR Clothing Minimum Arc Rating of 4 (See NFPA 70E 130.7(C)(10) for additional PPE)
Shock Hazard when cover is removed
Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 20мcC9101 (20мCC9101)
8-FDR TO 20MCC9101

Scenario 1 - Utility Power
Study Performed By PowerStudies.com (253) 639-8535


## Arc Flash and Shock Hazard

24 Ft 7 In
118
Dangerous!
Flash Hazard Boundary cal/ $\mathrm{cm}^{2}$ Flash Hazard at 1 Ft 6 In No PPE Exists - Do Not Work on Equipment while Energized!
480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:
Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 30SWbD9001 (30SWBD9001)
10-FDR TO 9002 12-30SWBD9001 MN
Line Side of:
Scenario 1-Utility Power
Study Performed By PowerStudies.com (253) 639-8535

## WARNING

## Arc Flash and Shock Hazard

5 Ft 6 In
10
Category 3

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In FR Clothing Minimum Arc Rating of 25 (See NFPA 70E 130.7(C)(10) for additional PPE)
Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 30SWBD9001 (30SWBD9001) 12-30SWBD9001 MN

Scenario 1-Utility Power

1 Ft 6 In
1.2

Category 1
480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:


Arc Flash and Shock Hazard
Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In FR Clothing Minimum Arc Rating of 4 (See NFPA 70E 130.7(C)(10) for additional PPE)
Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a $30 V F D 1001$ (30VFD1001)
13-FDR TO 30VFD1001

Scenario 1-Utility Power

## Arc Flash and Shock Hazard

## 1 Ft 6 In <br> 1.2

Category 1

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In FR Clothing Minimum Arc Rating of 4 (See NFPA 70E 130.7(C)(10) for additional PPE)
Shock Hazard when cover is removed
Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 30VFD1002 (30VFD1002)
FDR TO 30VFD1002

Scenario 1 - Utility Power
Study Performed By PowerStudies.com (253) 639-8535

## WARNING

## Arc Flash and Shock Hazard

1 Ft 1 In
0.71

Category 0
480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary
cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In
Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 30VFD8601 (30VFD8601)
FDR TO 30MTS8601

Scenario 1 - Utility Power
Study Performed By PowerStudies.com (253) 639-8535

## WARNING

## Arc Flash and Shock Hazard

1 Ft 2 In
0.75

Category 0

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 30VFD7600 (30VFD7600)
FDR TO 30VFD7600

Scenario 1-Utility Power

|  |  |
| :---: | :---: |
| Arc Flash and Shock Hazard |  |
| 2 Ft 7 ln | Flash Hazard Boundary |
| 2.9 | cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In |
| Category 1 | FR Clothing Minimum Arc Rating of 4 (See NFPA 70E 130.7(C)(10) for additional PPE) |
| 480 VAC | Shock Hazard when cover is removed |
| 00 | Glove Class |
| 3 Ft 6 ln | Limited Approach (Fixed Circuit) |
| 12 In | Restricted Approach |
| 1 In | Prohibited Approach |
| 04/28/2011 | Arc Flash Study Date IEEE 1584-2004a |
| Equipment ID (Name): | 40SWBD9101 (40SWBD9101) |
| Protective Device: | 26-FDR TO 40SWBD9101 |

Scenario 1-Utility Power

## Arc Flash and Shock Hazard

## 1 Ft 7 In <br> 1.3

Category 1

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In FR Clothing Minimum Arc Rating of 4 (See NFPA 70E 130.7(C)(10) for additional PPE)
Shock Hazard when cover is removed
Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 45VFD1001 (45VFD1001)
20-FDR TO 45VFD1001

Scenario 1 - Utility Power
Study Performed By PowerStudies.com (253) 639-8535

## WARNING

## Arc Flash and Shock Hazard

1 Ft 4 In
0.95

Category 0

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary
cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 45VFD1006 (45VFD1006)
23-FDR TO 45VFD1006

1 Ft 7 In
1.3

Category 1

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Arc Flash and Shock Hazard

## WARNING

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In FR Clothing Minimum Arc Rating of 4 (See NFPA 70E 130.7(C)(10) for additional PPE)
Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 45VFD1003 (45VFD1003) FDR TO 45VFD1003

Scenario 1-Utility Power


Arc Flash and Shock Hazard

1 Ft 3 In
0.93

Category 0

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In Non Melting Clothing (See NFPA 70E 130.7(C)(10) for additional PPE)

Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 45VFD1007 (45VFD1007)
FDR TO 45VFD1007

Scenario 1 - Utility Power

## WARNING

## Arc Flash and Shock Hazard

5 Ft 10 In
11
Category 3

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In FR Clothing Minimum Arc Rating of 25 (See NFPA 70E 130.7(C)(10) for additional PPE)
Shock Hazard when cover is removed
Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 46SWBD9101 (46SWBD9101)
19-FDR TO 46SWBD9101

Scenario 1 - Utility Power
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Arc Flash and Shock Hazard
26 Ft 9 In
135
Dangerous!
Flash Hazard Boundary
cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In
No PPE Exists - Do Not Work on Equipment while Energized!
480 VAC
00
3 Ft 6 In
12 In
Shock Hazard when cover is removed
Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a
46SWGR9001 (46SWGR9001)
16-FDR TO 9004
18-46SWGR9001 MN
ment ID (Name):
Protective Device:
Scenario 1 - Utility Power
Study Performed By PowerStudies.com (253) 639-8535

## WARNING

## Arc Flash and Shock Hazard

## 8 Ft 1 In

19
Category 3

480 VAC
00
3 Ft 6 In
12 In
1 In
04/28/2011
Equipment ID (Name):
Protective Device:

Flash Hazard Boundary cal/cm ${ }^{2}$ Flash Hazard at 1 Ft 6 In FR Clothing Minimum Arc Rating of 25 (See NFPA 70E 130.7(C)(10) for additional PPE)
Shock Hazard when cover is removed Glove Class
Limited Approach (Fixed Circuit)
Restricted Approach
Prohibited Approach
Arc Flash Study Date IEEE 1584-2004a 46SWGR9001 (46SWGR9001) 18-46SWGR9001 MN

Scenario 1-Utility Power

TAB 14

Project Name: 1104042-1

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Phase
Manufacturer: S\&C
Description: 15E-200E Slow Speed
Type: SMU-20, 25kV E-Rated
AIC Rating: 13kA Fault Duty: 4117.8A
Cartridge: SMU-20, 150E 16500V 150A Curve Multiplier: 1
Time Multiplier: $1 \quad$ Time Adder: 0
Size: 150A


| Device Name: | FDR TO 10XFMR9201 | TCC Name: |  |
| :---: | :---: | :---: | :---: |
| Bus Name: | 10DP9201 | Bus Voltage: | 480.0V |
| Function Name: | Phase |  |  |
| Manufacturer: | CUTLER-HAMMER |  |  |
| Description: | 15-225A |  |  |
| Type: | FD |  |  |
| AIC Rating: | 25kA | Fault Duty: | 22009.1A |
| Frame: | FD 480V 30A | Curve Multiplier: | 1 |
| Time Multiplier: | 1 | Time Adder: | 0 |
| Trip: | 30A |  |  |
| Setting: 1) Fixed |  |  |  |
| Device Name: | 5-FDR TO 10P1001 | TCC Name: | $1-\mathrm{Fdr}$ to |
| Bus Name: | 10SWBD9101 | Bus Voltage: | 480.0V |
| Function Name: | Phase |  |  |
| Manufacturer: | SIEMENS |  |  |
| Description: | 200-400A |  |  |
| Type: | HJXD6-A Sentron |  |  |
| AIC Rating: | 65kA | Fault Duty: | 25864.7A |
| Frame: | HJXD6-A 480V 300A | Curve Multiplier: | 1 |
| Time Multiplier: | 1 | Time Adder: | 0 |

Trip: 300A

Setting: 1) Thermal Curve (Fixed
2) INST (LO-HI) LO (1250A)

| Device Name: | FDR TO 10DP9201 | TCC Name: |  |
| :--- | :--- | :--- | :--- |
| Bus Name: | 10SWBD9101 | Bus Voltage: | 480.0V |
| Function Name: | Phase |  |  |
| Manufacturer: | SIEMENS |  |  |
| Description: | 70-250A |  |  |
| Type: | HFXD6 Sentron | Fault Duty: | 25864.7 A |
| AIC Rating: | 65kA | Curve Multiplier: 1 |  |
| Frame: | HFXD6 480V 150A | Time Adder: | 0 |

Trip: 150A
Setting: 1) Thermal Curve (Fixed HI
2) INST (LO-HI) (1500A)

| Device Name: | FDR TO 10P1002 | TCC Name: |  |
| :--- | :--- | :--- | :--- |
| Bus Name: | 10SWBD9101 | Bus Voltage: | 480.0 V |
| Function Name: | Phase |  |  |
| Manufacturer: | SIEMENS |  |  |
| Description: | 200-400A |  |  |
| Type: | HJXD6-A Sentron | Fault Duty: | 25864.7 A |
| AIC Rating: | 65kA | Curve Multiplier: 1 |  |
| Frame: | HJXD6-A 480V 300A | Time Adder: | 0 |

$\begin{array}{ll}\text { Time Multiplier: } \\ \text { Trip: } & 1 \\ 300 \mathrm{~A}\end{array}$
Setting: 1) Thermal Curve (Fixed
2) INST (LO-HI) LO (1250A)

| Device Name: | FDR TO 10 |  |  | TCC Name: |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Bus Name: | 10SWBD910 |  |  | Bus Voltage: | 480.0V |
| Function Name: | Phase |  |  |  |  |
| Manufacturer: | SIEMENS |  |  |  |  |
| Description: | 200-400A |  |  |  |  |
| Type: | HJXD6-A |  |  |  |  |
| AIC Rating: | 65 kA |  |  | Fault Duty: | 25864.7A |
| Frame: | HJXD6-A |  |  | Curve Multiplier: | 1 |
| Time Multiplier: | 1 |  |  | Time Adder: | 0 |
| Trip: | 300A |  |  |  |  |
| Setting: 1) Ther <br> 2) INST | nal Curve (LO-HI) | LO | (1250A) |  |  |
| Device Name: | FDR TO 70 |  |  | TCC Name: |  |
| Bus Name: | 10SWBD910 |  |  | Bus Voltage: | 480.0V |
| Function Name: | Phase |  |  |  |  |
| Manufacturer: | SIEMENS |  |  |  |  |
| Description: | 70-250A |  |  |  |  |
| Type: | HFXD6 Sen |  |  |  |  |
| AIC Rating: | 65 kA |  |  | Fault Duty: | 25864.7A |
| Frame: | HFXD6 480 |  |  | Curve Multiplier: | 1 |
| Time Multiplier: |  |  |  | Time Adder: | 0 |
| Trip: | 225A |  |  |  |  |
| Setting: 1) Ther <br> 2) INST | nal Curve (LO-HI) | HI | (2500A) |  |  |


Trip: 250A

Setting: 1) Thermal Curve (Fixed
2) INST (5-10x) 5 X (1250A)

| Device Name: | 10VFD1002 BRK |  |  | TCC Name: |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Bus Name: | 10VFD1002 |  |  | Bus Voltage: | 480.0V |
| Function Name: | Phase |  |  |  |  |
| Manufacturer: | ALLEN-BRADLEY |  |  |  |  |
| Description: | 90-250A |  |  |  |  |
| Type: | 140U-J, J-Frame |  |  |  |  |
| AIC Rating: | 65kA |  |  | Fault Duty: | 24195.0A |
| Frame: | 140U-J 480V 250A |  |  | Curve Multiplier: | 1 |
| Time Multiplier: | 1 |  |  | Time Adder: | 0 |
| Trip: | 250A |  |  |  |  |
| Setting: 1) Ther <br> 2) INST | mal Curve (Fixed (5-10x) | 5X | (1250A) |  |  |



Function Name: Ground
Manufacturer: SIEMENS
Description: GF, 200-3200AP
Type:
WL, ETU745, Size II
AIC Rating: 100kA ShortTime: 100
WLL, Size II 508V 3200A
Fault Duty: $\quad 28649.6 \mathrm{~A}$
Frame:
$\begin{array}{ll}\text { Time Multiplier: } & 1 \\ \text { Sensor: } & 3200 \mathrm{~A}\end{array}$
Plug: 1600A
Setting: 1) Ig, (100-1200A) D (900A)
2) $\mathrm{tg},(0.1-0.5 \mathrm{~s}) 2 \mathrm{I} 2 \mathrm{t}$ In


| Function Name: Gournd |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Manufacturer: | SIEMENS |  |  |  |  |
| Description: | GF, 200-3200AP |  |  |  |  |
| Type: | WL, ETU745, Size II |  |  |  |  |
| AIC Rating: | 100kA ShortTime: 100 |  |  | Fault Duty: | 28649.6A |
| Frame: | WLL, Size II 508V 3200A |  |  | Curve Multiplier: | 1 |
| Time Multiplier |  |  |  | Time Adder: | 0 |
| Sensor: | 3200A |  |  |  |  |
| Plug: | 1000A |  |  |  |  |
| Setting: 1) Ig, | (100-1200A) | C | (600A) |  |  |
| 2) tg , | (0.1-0.5s) | 1 | $\mathrm{I}^{\wedge} 2 \mathrm{t}$ In |  |  |


| Device Name: | 8-FDR TO 20MCC9101 |  |  | TCC Name: | 2-15SWGR900 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Bus Name: | 15SWGR9001 |  |  | Bus Voltage: | 480.0 V |
| Function Name: | : Phase |  |  |  |  |
| Manufacturer: | SIEMENS |  |  |  |  |
| Description: | LSI, 200-3200AP |  |  |  |  |
| Type: | WL, ETU745, Size II |  |  |  |  |
| AIC Rating: | 100kA Override:100 ShortTime:85 |  |  | Fault Duty: | 28649.6A |
| Frame: | WLL, Size II 508V 1600A |  |  | Curve Multiplier: | 1 |
| Time Multiplier | ier: 1 |  |  | Time Adder: | 0 |
| Sensor: | 1600A |  |  |  |  |
| Plug: | 600A |  |  |  |  |
| Setting: 1) LTP | LTPU, (0.4-1 x P) | 1 | (600A) |  |  |
| 2) LTD | LTD-I2t, (2-30s) | 3.5 |  |  |  |
| 3) STP | STPU, (1.25-12 x P | 3 | (1800A) |  |  |
| 4) STD | STD, (0.1-0.4 x P ) | 0.1 I | $\mathrm{I}^{\wedge} 2 \mathrm{t}$ Out |  |  |
| 5) INS | INST, (1.5-12 x P), | 12 | (7200A) |  |  |


| Function Name: | Ground |
| :--- | :--- |
| Manufacturer: | SIEMENS |
| Description: | GF, 200-3200AP |
| Type: | WL, ETU745, Size II |
| AIC Rating: | 100kA ShortTime:100 |
| Frame: | WLL, Size II 508V 1600A |
| Time Multiplier: | 1 |
| Sensor: | 1600A |
| Plug: | 600A |
| Setting: 1) $\operatorname{Ig}$, | $(100-1200 \mathrm{~A})$ |
|  | 2) tg, |
|  | $(0.1-0.5 \mathrm{~s})$ |
|  | B |


| Device Name: | FDR TO 20XFMR9201 | TCC Name: |  |
| :---: | :---: | :---: | :---: |
| Bus Name: | 20DP9201 | Bus Voltage: | 480.0V |
| Function Name: | Phase |  |  |
| Manufacturer: | CUTLER-HAMMER |  |  |
| Description: | 15-225A |  |  |
| Type: | FD |  |  |
| AIC Rating: | 25kA | Fault Duty: | 16059.2A |
| Frame: | FD 480V 30A | Curve Multiplier: | 1 |
| Time Multiplier: | 1 | Time Adder: | 0 |
| Trip: | 30A |  |  |
| Setting: 1) Fixed |  |  |  |


Trip:
150A

Setting: 1) Thermal Curve (Fixed
2) INST (5X - 10X x In) 10X (1500A)

| Device Name: | FDR TO 20DP9201 | TCC Name: |  |
| :---: | :---: | :---: | :---: |
| Bus Name: | 20MCC9101 | Bus Voltage: | 480.0V |
| Function Name: | Phase |  |  |
| Manufacturer: | ALLEN-BRADLEY |  |  |
| Description: | 15-150A, 3 Pole |  |  |
| Type: | 140U-I3, I6 |  |  |
| AIC Rating: | 35kA | Fault Duty: | 25546.9A |
| Frame: | 140U-I3 480V 30A | Curve Multiplier: | 1 |
| Time Multiplier: | 1 | Time Adder: | 0 |

Trip: 30 A

Setting: 1) Opening Clearing Cur

| Device Name: | FDR TO 30XFMR9201 | TCC Name: |  |
| :--- | :--- | :--- | :--- |
| Bus Name: | 30DP9201 | Bus Voltage: | 480.0 V |
| Function Name: | Phase |  |  |
| Manufacturer: | CUTLER-HAMMER |  |  |
| Description: | 15-225A |  |  |
| Type: | FD | Fault Duty: | 13015.7A |
| AIC Rating: | 25 kA | Curve Multiplier: 1 |  |
| Frame: | FD 480V 50A | Time Adder: | 0 |
| Time Multiplier: 1 |  |  |  |
| Trip: | 50 A |  |  |
| Setting: 1) Fixed |  |  |  |



| Function Name: | Ground |  |  |
| :---: | :---: | :---: | :---: |
| Manufacturer: | SIEMENS |  |  |
| Description: | GF, 200-3200AP |  |  |
| Type: | WL, ETU745, Size II |  |  |
| AIC Rating: | 100kA ShortTime:100 |  |  |
| Frame: | WLL, Size II 508V 3200A |  |  |
| Time Multiplier | 1 |  |  |
| Sensor: | 3200A |  |  |
| Plug: | 2000A |  |  |
| Setting: 1) Ig, | (100-1200A) | E | (1200A) |
| 2) tg , | (0.1-0.5s) | 1 | $\mathrm{I}^{\wedge} 2 \mathrm{t}$ I |


| Device Name: | 13-FDR TO 30VFD1001 |  | TCC Name: | 3-Fdr to |
| :---: | :---: | :---: | :---: | :---: |
| Bus Name: | 30SWBD9001 |  | Bus Voltage: | 480.0V |
| Function Name: | Phase |  |  |  |
| Manufacturer: | SIEMENS |  |  |  |
| Description: | 800-1200A |  |  |  |
| Type: | NG, 525 |  |  |  |
| AIC Rating: | 65 kA |  | Fault Duty: | 30586.6A |
| Frame: | HNG 480V 1000A |  | Curve Multiplier: | 1 |
| Time Multiplier: | 1 |  | Time Adder: | 0 |
| Trip: | 1000A |  |  |  |
| Setting: 1) Therm <br> 2) INST | $\begin{aligned} & \text { mal Curve (Fixed } \\ & (5-10 \mathrm{kA}) \end{aligned}$ | ( 5000A) |  |  |


| Device Name: | FDR TO 30DP9201 | TCC Name: |
| :--- | :--- | :--- |
| Bus Name: | 30SWBD9001 | Bus Voltage: | 480.0V

$\begin{array}{ll}\text { Time Multiplier: } 1 \\ \text { Trip: } & 150 \mathrm{~A}\end{array}$
Setting: 1) Thermal Curve (Fixed
2) INST (LO-HI) HI (1500A)



| Device Name: | 30VFD7600 BRK |  |  | TCC Name: |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Bus Name: | 30VFD7600 |  |  | Bus Voltage: | 480.0V |
| Function Name: | Phase |  |  |  |  |
| Manufacturer: | ALLEN-BRADLEY |  |  |  |  |
| Description: | 90-250A |  |  |  |  |
| Type: | 140U-J, J-Frame |  |  |  |  |
| AIC Rating: | 65kA |  |  | Fault Duty: | 28222.1A |
| Frame: | 140U-J 480V 250A |  |  | Curve Multiplier: | 1 |
| Time Multiplier: | 1 |  |  | Time Adder: | 0 |
| Trip: | 250A |  |  |  |  |
| Setting: 1) Ther <br> 2) INST | mal Curve (Fixed (5-10x) | 5X | (1250A) |  |  |


| Device Name: | 30VFD8601 BRK |  | TCC Name: |  |
| :---: | :---: | :---: | :---: | :---: |
| Bus Name: | 30VFD8601 |  | Bus Voltage: | 480.0V |
| Function Name: | Phase |  |  |  |
| Manufacturer: | ALLEN-BRADLEY |  |  |  |
| Description: | 90-250A |  |  |  |
| Type: | 140U-J, J-Frame |  |  |  |
| AIC Rating: | 65kA |  | Fault Duty: | 25504.1A |
| Frame: | 140U-J 480V 250A |  | Curve Multiplier: | 1 |
| Time Multiplier: | 1 |  | Time Adder: | 0 |
| Trip: | 250A |  |  |  |
| Setting: 1) Thermal Curve (Fixed <br> 2) INST (5-10x) |  | (1250A) |  |  |
| Device Name: | FDR TO 40XFMR9201 |  | TCC Name: |  |
| Bus Name: | 40DP9201 |  | Bus Voltage: | 480.0V |
| Function Name: | Phase |  |  |  |
| Manufacturer: | CUTLER-HAMMER |  |  |  |
| Description: | 15-225A |  |  |  |
| Type: | FD |  |  |  |
| AIC Rating: | 25kA |  | Fault Duty: | 26416.5A |
| Frame: | FD 480V 30A |  | Curve Multiplier: | 1 |
| Time Multiplier: |  |  | Time Adder: | 0 |
| Trip: | 30A |  |  |  |
| Setting: 1) Fixed |  |  |  |  |
| Device Name: | FDR TO 40XFMR9202 |  | TCC Name: |  |
| Bus Name: | 40DP9202 |  | Bus Voltage: | 480.0V |
| Function Name: | Phase |  |  |  |
| Manufacturer: | CUTLER-HAMMER |  |  |  |
| Description: | 15-225A |  |  |  |
| Type: | FD |  |  |  |
| AIC Rating: | 25kA |  | Fault Duty: | 11428.8A |
| Frame: | FD 480V 60A |  | Curve Multiplier: | 1 |
| Time Multiplier: | 1 |  | Time Adder: | 0 |
| Trip: | 60A |  |  |  |
| Setting: 1) Fixed |  |  |  |  |






| Device Name: | FDR TO 40DP9202 |  |  | TCC Name: |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Bus Name: | 46SWBD9101 |  |  | Bus Voltage: | 480.0V |
| Function Name: | Phase |  |  |  |  |
| Manufacturer: | SIEMENS |  |  |  |  |
| Description: | 70-250A |  |  |  |  |
| Type: | HFXD6 Sentron |  |  |  |  |
| AIC Rating: | 65 kA |  |  | Fault Duty: | 33777.2A |
| Frame: | HFXD6 480V 150A |  |  | Curve Multiplier: | 1 |
| Time Multiplier: | 1 |  |  | Time Adder: | 0 |
| Trip: | 150A |  |  |  |  |
| Setting: 1) Ther <br> 2) INST | mal Curve (Fixed (LO-HI) | HI | (1500A) |  |  |
| Device Name: | FDR TO 45VFD1003 |  |  | TCC Name: |  |
| Bus Name: | 46SWBD9101 |  |  | Bus Voltage: | 480.0V |
| Function Name: | Phase |  |  |  |  |
| Manufacturer: | SIEMENS |  |  |  |  |
| Description: | 800-1200A |  |  |  |  |
| Type: | NG, 525 |  |  |  |  |
| AIC Rating: | 65kA |  |  | Fault Duty: | 33777.2A |
| Frame: | HNG 480V 1000A |  |  | Curve Multiplier: | 1 |
| Time Multiplier: | 1 |  |  | Time Adder: | 0 |
| Trip: | 1000A |  |  |  |  |
| Setting: 1) Ther <br> 2) INST | mal Curve (Fixed (5-10kA) | 5000 | (5000A) |  |  |
| Device Name: | FDR TO 45VFD1007 |  |  | TCC Name: |  |
| Bus Name: | 46SWBD9101 |  |  | Bus Voltage: | 480.0V |
| Function Name: | Phase |  |  |  |  |
| Manufacturer: | SIEMENS |  |  |  |  |
| Description: | 200-400A |  |  |  |  |
| Type: | HJXD6-A Sentron |  |  |  |  |
| AIC Rating: | 65kA |  |  | Fault Duty: | 33777.2A |
| Frame: | HJXD6-A 480V 400A |  |  | Curve Multiplier: | 1 |
| Time Multiplier: |  |  |  | Time Adder: | 0 |
| Trip: | 350A |  |  |  |  |
| Setting: 1) Ther <br> 2) INST | mal Curve (Fixed (LO-HI) | LO | (2000A) |  |  |
| Device Name: | FDR TO 50DP9201 |  |  | TCC Name: |  |
| Bus Name: | 46SWBD9101 |  |  | Bus Voltage: | 480.0V |
| Function Name: | Phase |  |  |  |  |
| Manufacturer: | SIEMENS |  |  |  |  |
| Description: | 70-250A |  |  |  |  |
| Type: | HFXD6 Sentron |  |  |  |  |
| AIC Rating: | 65kA |  |  | Fault Duty: | 33777.2A |
| Frame: | HFXD6 480V 250A |  |  | Curve Multiplier: | 1 |
| Time Multiplier: |  |  |  | Time Adder: | 0 |
| Trip: | 225A |  |  |  |  |
| Setting: 1) Ther <br> 2) INST | mal Curve (Fixed (LO-HI) | HI | (2500A) |  |  |



| Function Name: Ground |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Manufacturer: | SIEMENS |  |  |  |  |
| Description: | GF, 800-5000AP |  |  |  |  |
| Type: | WL, ETU745, Size III |  |  |  |  |
| AIC Rating: | 100kA ShortTime: 100 |  |  | Fault Duty: | 35434.3A |
| Frame: | WLL, Size III 508V 4000A |  |  | Curve Multiplier: | 1 |
| Time Multiplier | 1 |  |  | Time Adder: | 0 |
| Sensor: | 4000A |  |  |  |  |
| Plug: | 2500A |  |  |  |  |
| Setting: 1) Ig, | (400-1200A) | E | (1200A) |  |  |
| 2) tg , | (0.1-0.5s) | 2 | $\mathrm{I}^{\wedge} 2 \mathrm{t}$ In |  |  |


Function Name: Ground

Manufacturer: SIEMENS
Description: GF, 800-5000AP
Type: WL, ETU745, Size III
AIC Rating: 100kA ShortTime:100 Fault Duty: 35434.3A
Frame: WLL, Size III 508V 4000A Curve Multiplier: 1
Time Multiplier: 1
Sensor: 4000A
Plug: 2000A
Setting: 1) Ig, (400-1200A) C (800A)
2) $\mathrm{tg},(0.1-0.5 \mathrm{~s}) 1 \quad \mathrm{I}^{\wedge} 2 \mathrm{t} \mathrm{In}$


| Function Name: | Ground |  |  |
| :---: | :---: | :---: | :---: |
| Manufacturer: | SIEMENS |  |  |
| Description: | GF, 200-1200AP |  |  |
| Type: | WL, ETU745, Size I |  |  |
| AIC Rating: | 100kA ShortTime:100 |  |  |
| Frame: | WLL, Size I 508V 800A |  |  |
| Time Multiplier |  |  |  |
| Sensor: | 800A |  |  |
| Plug: | 600A |  |  |
| Setting: 1) Ig, | (100-1200A) | B | (300A) |
| 2) tg , | (0.1-0.5s) | 0.1 | I^2 t In |


| Device Name: | 50DP9201 MAIN | TCC Name: |  |
| :--- | :--- | :--- | :--- |
| Bus Name: | 50DP9201 | Bus Voltage: | 480.0 V |
| Function Name: | Phase |  |  |
| Manufacturer: | CUTLER-HAMMER |  |  |
| Description: | 15-225A |  |  |
| Type: | FD | Fault Duty: | 10532.8A |
| AIC Rating: | 25 kA | Curve Multiplier: 1 |  |
| Frame: | FD 480V 225A | Time Adder: | 0 |
| Time Multiplier: | 1 |  |  |
| Trip: | 225 A |  |  |
| Setting: 1) Fixed |  |  |  |


| Device Name: | FDR TO 50XFMR9201 | TCC Name: |  |
| :--- | :--- | :--- | :--- |
| Bus Name: | 50DP9201 | Bus Voltage: | 480.0 V |
| Function Name: | Phase |  |  |
| Manufacturer: | CUTLER-HAMMER |  |  |
| Description: | 15-225A |  |  |
| Type: | FD | Fault Duty: | 10532.8A |
| AIC Rating: | 25 kA | Curve Multiplier: 1 |  |
| Frame: | FD 480V 60A | Time Adder: | 0 |
| Time Multiplier: 1 |  |  |  |
| Trip: |  |  |  |
| Setting: 1) Fixed |  |  |  |



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Please go to the Salisbury website to look at PPE gear and download a catalog. http://www.whsalisbury.com/arc/arc.htm


[^0]:    *     - Use these settings above if no other settings are specified on the following device setting sheets.

[^1]:    Study Performed By PowerStudies.com (253) 639-8535

[^2]:    Study Performed By PowerStudies.com (253) 639-8535

